

LAND OFF SHEPPEY WAY, IWADE

SURFACE WATER MANAGEMENT STATEMENT

MIDDLEFIELDS LTD

SEPTEMBER 2019



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1. EXECUTIVE SUMMARY

- 1.1. This Surface Water Management Statement has been prepared in connection with proposals for 14 retirement cottages for sheltered accommodation on land off Sheppey Way, Iwade.
- 1.2. The site lies entirely within Flood Zone 1.
- 1.3. The site is undeveloped and the available evidence identifies that the use of soakaways will not provide a suitable means of draining surface water runoff from development on the site. It will therefore be necessary to use flow balancing methods in order to store and attenuate surface water runoff to the greenfield runoff rates which in this instance is a minimum practicable controlled flow rate of 2 l/s.
- 1.4. The required storage will be provided using oversized pipes and an underground geocellular tank. Outflow from the storage facilities is controlled by means of suitable vortex flow control device before discharge to an offsite sewer. Car parking bays will be formed of 'lined' pervious pavement as a means of a collection of rainfall / runoff and as Source Control.
- 1.5. The overall conclusions drawn from this Surface Water Management Statement are that a suitable means of drainage can be provided to serve the proposed development in terms of the disposal of surface water runoff.

2. INTRODUCTION

- 2.1. This Surface Water Management Statement has been prepared on behalf of Middlefields Ltd in connection with proposals for residential development on land off Sheppey Way, Iwade.
- 2.2. The overall site comprises around 0.38 hectares, and is located to the west of Sheppey Way to the south of the village of Iwade, which lies in the Borough of Swale. The post code is ME9 8TY, and the approximate grid reference for the site is 589913, 167119. The location of the site is shown edged red on **Figure 1** below and lies entirely within Flood Zone 1.

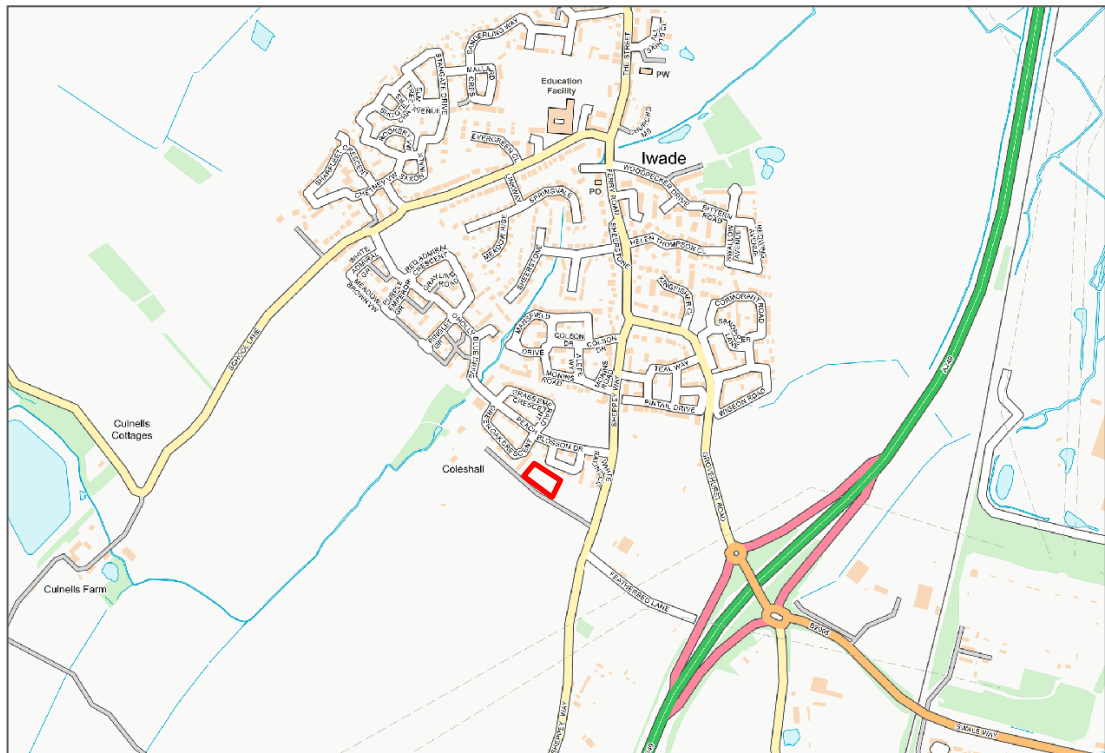


Figure 1: Site Location Plan

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- 2.3. The main purpose of this Surface Water Management Statement is to provide sufficient information in support of a planning application to demonstrate that a suitable means of drainage can be provided to serve the proposed development in terms of the disposal of surface water runoff.

3. SITE CONTEXT

Site Description and Site Levels

- 3.1. The site is currently undeveloped in agricultural use and bounded by a new housing estate to north of the site and agricultural land and hedgerow to the south.
- 3.2. The nearest watercourse is the Iwade Stream which is situated 0.2km to the northwest of the site. The Iwade Stream flows from southwest to northeast through the village of Iwade which is designated as a 'main river'.
- 3.3. A Topographical Survey was undertaken by J. C. White in June 2019 and a copy of Drawing Number 19/00/060/1 is reproduced in **Appendix 1**. The Topographical Survey indicates that the site falls from a high point of approximately 18.60m Above Ordnance Datum (AOD) towards the northwestern boundary at 18.3m AOD and Sheppey Way at 17.70m AOD.
- 3.4. No formal drainage features (ditches or sewers) are identified on the site based on the desktop information reviewed.

Ground Conditions

- 3.5. The British Geological Survey (BGS) geological mapping of the area shows the site is underlain by London Clay Formation (clay and silt) bedrock and Head (clay and silt) superficial deposits.
- 3.6. Based on the Flood Studies Report Winter Rainfall Acceptance Potential (WRAP) Map, as shown reproduced on Drawing Number P912/01 in **Appendix 2**, the site is located in a 'Soil Index Class 4' area. Soil Index Class 4 has a low winter rainfall acceptance potential and a high standard percentage runoff, and so suggests the underlying soil has poor permeability.
- 3.7. The Cranfield Soil and AgriFood Institute (CSAI), incorporating the National Soil Resources Institute (NSRI,) at Cranfield University maintains soil reports and maps for England and Wales. The Soilscales dataset map indicates that the site lies on the boundary between 'Loamy soils with naturally high groundwater' which are 'naturally wet' and 'Slowly permeable seasonally wet slightly acid but base-rich loamy and clayey soils' which have 'impeded drainage'. After heavy rainfall, particularly during the winter, the subsoil becomes waterlogged, resulting in very wet ground conditions.

Groundwater Source Protection

- 3.8. From an inspection of the Environment Agency's Aquifer Designation Map on its website the site's underlying bedrock and superficial deposits are classified as 'Unproductive strata' which is defined as geological strata with low permeability that have negligible significance for water supply or river base flow. A copy of the Environment Agency's Aquifer Designation Map is reproduced in **Figure 2** below.

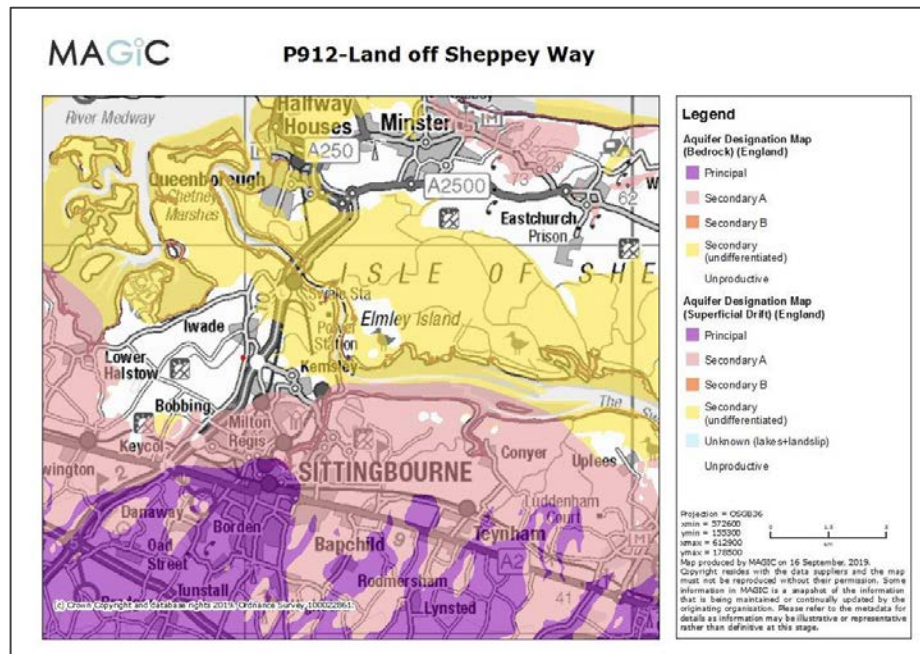


Figure 2: Environment Agency's Aquifer Designation Map

- 3.9. From an inspection of the Environment Agency's Groundwater Source Protection Zone Map the site does not fall within a Groundwater Source Protection Zone.

Flood Hazards

- 3.10. As the site is less than 1 hectare in Flood Zone 1 (which is land assessed as having a less than 1 in 1,000 annual probability of river or sea flooding) a formal site-specific flood risk assessment is not required to support a planning application for the proposed development. An examination of the Government's Flood Mapping data identifies that the site is not at risk of flooding from surface water or reservoirs.

Development Proposals

- 3.11. The development proposals comprise 14 retirement cottages for sheltered accommodation. A copy of the Proposed Site Plan, Drawing Number 766 P02, prepared by CDP Architecture Ltd, showing the development proposals, is reproduced in **Appendix 3**.

4. SURFACE WATER DRAINAGE STRATEGY

Design Criteria

Climate Change

- 4.1. The NPPF requires development to take account of the impacts of climate change. The allowances to be made for climate change effects when assessing flood risk and designing drainage systems are related to the lifetime of the development. Residential development should be considered for a life of a minimum of 100 years¹.
- 4.2. The peak rainfall intensity allowances to be used when designing urban drainage systems are given in Table 2 of guidance published by the Environment Agency in February 2019². Both the central and upper end allowances need to be assessed to understand the range of impact. The total potential change anticipated for 2060 to 2115 is 20% for the central category, and 40% for the upper end category.

Standard of Protection

- 4.3. In terms of providing an acceptable standard of protection against flooding for new development, paragraph 54³ in the Flood Risk and Coastal Change Planning Practice Guidance that no flooding of property should occur as a result of the 'design flood' corresponding to a 1 in 100 year fluvial flood event, or a 1 in 200 tidal flood event, taking account of climate change⁴.
- 4.4. The Government published its 'Non-statutory technical standards for sustainable drainage systems' in March 2015. They should be used in conjunction with the NPPF and planning practice guidance. Standard S7 states that the drainage system must be designed so that flooding does not occur on any part of the site for a 1 in 30 year rainfall event. Standard S8 goes on to state that the drainage system must be designed so that flooding does not occur during a 1 in 100 year rainfall event in any part of a building (including a basement); or in any utility plant susceptible to water within the development.

Sustainable Drainage Systems

- 4.5. Paragraph 51⁵ in the Flood Risk and Coastal Change Planning Practice Guidance advises that sustainable drainage systems are designed to control surface water runoff close to where it falls and mimic natural drainage as closely as possible. Sustainable drainage systems provide opportunities to:
- reduce the causes and impacts of flooding;
 - remove pollutants from urban runoff at source;
 - combine water management with green space with benefits for amenity, recreation and wildlife.

¹ Planning Practice Guidance Reference ID: 7-026-20140306

² Environment Agency (February 2019) 'Flood risk assessments: climate change allowances'

³ Planning Practice Guidance Reference ID: 7-054-20150415

⁴ Planning Practice Guidance Reference ID: 7-055-20140306

⁵ Planning Practice Guidance Reference ID: 7-051-20150323

4.6. The Guidance⁶ advises that, generally, the aim should be to discharge surface water runoff as high up the following hierarchy of drainage options as reasonably practicable:

- into the ground (infiltration);
- to a surface water body;
- to a surface water sewer, highway drain, or another drainage system;
- to a combined sewer.

4.7. Section 3.2 of Approved Document H of the Building Regulations also promotes the drainage hierarchy.

4.8. The 'Non-statutory technical standards for sustainable drainage systems' relates to the design, construction, operation and maintenance of sustainable drainage systems and have been published as guidance. The Government expect these standards to apply to all developments of 10 homes or more and so are applicable to this scheme.

Surface Water Management

4.9. A sustainable drainage strategy, involving the implementation of SuDS, is proposed for managing the disposal of surface water runoff from the proposed development on the site. The strategy has regard to the advice in CIRIA C753 'The SuDS Manual' and Kent County Council's requirements as set out in its 'Drainage and Policy Statement'.

4.10. Based on the ground conditions discussed above the use of soakaways will not provide a suitable means of draining surface water runoff from development on the site. It is therefore necessary to use flow balancing methods in order to store and attenuate surface water runoff to greenfield runoff rates (or minimum practicable controlled flow rate of 2 l/s).

Greenfield Runoff

4.11. The ICP SuDS module in the MicroDrainage design software enables the calculation of greenfield runoff rates based on the IH124 estimation method with pro-rata values for sites smaller than 50ha. Rainfall and soil parameters have been obtained from maps in Volume V of the Flood Studies Report (FSR) within the MicroDrainage Source Control software. FSSR 2 and 14 regional growth curve factors are used to calculate the greenfield peak flow rates for 1, 30 and 100 year return periods.

4.12. The FSR WRAP Map, shown in **Appendix 2**, indicates the site is located in 'Soil Index Class 4'. A Soil Index value of 0.45 has there been used to calculate Q_{BAR} in IH Report 124.

4.13. Copies of the MicroDrainage greenfield runoff calculations for the site are included in **Appendix 4**. A summary of the greenfield runoff rates for the various return period events is shown in **Table A**. The mean annual peak rate of runoff, referred to as Q_{BAR} in IH Report 124, is 1.6 l/s.

Table A: Greenfield Runoff Rates

Return Period (Years)	1	Q_{BAR}	30	100
Greenfield Runoff Rates (l/s/ha)	3.4	4.0	9.1	12.9
Greenfield Runoff Rates (l/s)	1.3	1.6	3.6	5.0

⁶ Planning Practice Guidance Reference ID: 7-080-20150323

- 4.14. Kent County Council's 'Drainage and Policy Statement' sets the minimum achieved controlled flow rate of 2 l/s. This is due to constraints on the size of the hydraulic control unit while keeping the risk of blockage to an acceptable level.
- 4.15. As such it is proposed to limited the developed rate of runoff to 2 l/s, for all rainfall events up to the 100 year return period event, including an allowance for climate change, the proposed development would reduce flood risk overall when compared to existing greenfield rates.
- Attenuation Storage**
- 4.16. The required storage to achieve the restricted runoff rate will be provided using oversized pipes and underground geocellular tank. Outflow from the storage facilities is controlled by means of suitable vortex flow control device.
- 4.17. Car parking bays will be formed of 'lined' pervious pavement as a means of a collection of rainfall / runoff and as Source Control.
- 4.18. A direct outfall to the Iwade Stream some 200m to the north is not achievable and therefore a connection into the local sewer network in the development area to the north of the site is proposed.
- 4.19. Enquiries have been made to Southern Water to establish the location of the existing public sewers in the vicinity of the site. A copy of Southern Water's response and public sewer map are reproduced in **Appendix 5**. The Southern Water asset maps do not show any 'public' sewers in the development to the north of the site or in Sheppey Way. The sewers which serve the development site to the north have yet to be 'adopted' by Southern Water and therefore do not appear on their asset maps. Due to the presence of sewers to the north of the there is an adequate point of connection for the proposed development.
- 4.20. The land to the north was granted outline planning consent (planning reference: SW/08/1127) in June 2011. Drawing No. 690488/C/204 Rev A 'Section 104 Agreement Surface Water S104 Layout East System' was submitted as part of application reference SW/081127/CCH to comply with the planning conditions of the outline planning consent. The surface water drainage strategy makes allowance for a 5 l/s baseflow from the area of land which includes the application site. It is therefore concluded that the sewers in the development site to the north have been designed to take into account development on the application site. It is proposed to restrict the discharge rate from the proposed development to 2 l/s which is less than the 5 l/s capacity allowed for in the offsite sewer.
- 4.21. The proposed Care Home development (Ref: 19/501160/REM) to the east of the application site proposes to connect into the sewer system in the development area to the north at a controlled discharge rate of 1.4 l/s. If in due course the outflow rate from the proposed Care Home development is increased to 2 l/s then the peak flows from both development sites will be 4 l/s (which is less than 5 l/s allowed for). The offsite sewer in the development land to the north has been designed to take this flow rate into account.
- 4.22. A preliminary surface water drainage strategy is shown on the Preliminary Surface Water Drainage Strategy Plan, Drawing No. P912/02, a copy of which is contained in **Appendix 6**.
- 4.23. Pollution control measures include use of lined pervious pavement on car parking bays and use of deep trapped gullies in other road areas.

- 4.24. The proposed drainage strategy would ensure that surface water arising from the developed site would be managed in a sustainable manner to mimic the surface water flows arising from the site prior to the proposed development, while reducing the flood risk to the site itself and elsewhere, taking climate change into account.

SuDS Management Train

- 4.25. In terms of the SuDS 'management train', the drainage strategy for the proposed development seeks to address the quality and quantity of runoff as follows:-

i) Prevention

- 4.26. Prevention is the use of good site design and housekeeping measures to prevent pollution. Good site design includes the provision of pervious paving to retain sediment, and soft landscaping within the site to encourage evapotranspiration. The housekeeping measures cover maintenance of the drainage system and general site maintenance.

ii) Source Control

- 4.27. Source control is the control of runoff at or very near its source. The use of lined pervious pavements intercepts rainfall at source before discharging the runoff into the below ground attenuation system.

iii) Site Control

- 4.28. Site control is the management of water from several sub-catchments within a site. The proposed surface water drainage system amalgamates the runoff from the roofs, roads, and paved areas, for each area of development on the site, and deals with it in a combination of oversized pipes and a geocellular tank to reduce the rate of runoff from the site.

- 4.29. The pervious paving would contribute to the pollutant and sediment removal capability of the SuDS management train.

iv) Regional Control

- 4.30. Regional control is the management of runoff from more than one site and so in this case is covered by the site control techniques.

Surface Water Flow Balancing

- 4.31. The use of flow balancing methods, comprising oversized pipes and a geocellular tank is proposed in order to attenuate surface water runoff to the identified rate of 2 l/s with discharge to the local sewer system.

- 4.32. A Network model has been created in MicroDrainage, software system, and the 1 in 1, 30, 100 year events, plus 20% and 40% increases in peak rainfall intensity to take account of climate change, have been simulated. The outflow from the drainage system has been constrained to 2.0 l/s, and hence a reduced rate of runoff for higher return periods. Copies of the MicroDrainage simulation results are reproduced in **Appendix 7** and summarised in **Table B** below.

- 4.33. **Table B** shows the peak runoff rate from the development during the 1 in 1 year, 1 in 30, and 1 in 100 year rainfall events plus climate change, for the pre-development and post development situations.

Table B: Comparison of Runoff Rates and Attenuation Storage Volumes

Storm Event	Pre Development 'Greenfield' Runoff Rate (l/s)	Allowable Discharge Rate (l/s)	Proposed Discharge Rate (l/s)	Attenuation Storage (m ³)*
1 in 1	1.3	2.0	1.2	7
1 in 30	3.6	2.0	1.2	36
1 in 100	5.0	2.0	1.4	61
1 in 100 + 20%	N/A	2.0	1.5	83
1 in 100 + 40%	N/A	2.0	1.6	105

Notes: * volume of attenuation storage utilised in geocellular tank and length of 900mm diameter pipe.

- 4.34. Accordingly the detailed engineering design of the site will need to demonstrate that a minimum of 105 m³ of surface water attenuation is proposed. The 30 year level of attenuation will be provided within the pipe system (to be adopted by Southern Water). The remaining level of attenuation will be provided within the permeable paving areas, including the car park surface, and will be demonstrated when the detailed designs are submitted and can be subject to an appropriate condition.
- 4.35. The proposed storage areas and oversized pipes which provided this level of attenuation are shown on the Preliminary Drainage Strategy Plan, Drawing No. P912/02 in Appendix 6, which indicates the location and sizes of the required storage facilities to serve the various development areas.
- 4.36. The above plan and calculations demonstrate that a suitable means of drainage can be provided to drain the developed site in terms of surface water runoff in accordance with the guidance and standards laid down.

Non-statutory technical standards for sustainable drainage systems

- 4.37. **Table C** demonstrates how the proposed development complies with the relevant standards of the Government's 'Non-statutory technical standards for sustainable drainage systems'.

Table C: Compliance with Non-statutory technical standards for sustainable drainage systems

Standard	Justification for compliance
Flood risk outside the development	
S1	N/A – discharge to a sewer.
Peak flow control	
S2	From inspection of Table B it can be seen that the peak runoff rate from the development to the offsite sewer for the 1 in 1 year rainfall event and the 1 in 100 year rainfall event never exceed the peak greenfield runoff rate for the same event.
S3	N/A - the site is a greenfield development.
Volume control	
S5	N/A – the site is a greenfield development so S4 and S6 apply.
S4 & S6	<p>As a result of the proposed development the amount of impermeable area increases which has implications for runoff volume.</p> <p>Ground conditions dictate that the use of infiltration drainage would be unsuitable and therefore would not be viable means to dispose of this additional volume.</p> <p>From inspection of Table B it can be seen that the runoff volume is discharged at a rate that does not adversely affect flood risk which equates to 2 l/s (the lowest practicable discharge rate).</p>

Flood Risk within the development	
S7	The surface water drainage system and site ground levels will be designed so that flooding does not occur on any part of the site for a 1 in 30 year rainfall event. The proposed geocellular tank and oversized pipes are sized to accommodate the 1 in 100 year rainfall event (including a 40% allowance for climate change) with no flooding. S7 is satisfied based on the calculations contained in Appendix 7.
S8	The surface water drainage system and site ground levels will be designed so that flooding does not occur on any part of the site for a 1 in 100 year rainfall event. The proposed geocellular tank and oversized pipes are sized to accommodate the 1 in 100 year rainfall event (including a 40% allowance for climate change) with no flooding. S8 is satisfied based on the calculations contained in Appendix 7.
S9	The design of the site ensures that, so far as is reasonably practicable, flows resulting from rainfall in excess of a 1 in 100 year rainfall event are managed in exceedance routes that minimise the risks to people and property.
Structural integrity	
S10	Components would be designed to ensure structural integrity of the drainage system under anticipated loading conditions over the design life of the development.
S11	The materials specified by the designer at the detailed design stage would be of a suitable nature and quality for their intended use.
Designing for maintenance considerations	
S12	N/A - Pumping is not proposed.
Construction	
S13	The mode of construction with the existing sewer would comply with the appropriate standards and be inspected by the relevant authority so would not be prejudicial to the structural integrity and functionally of the drainage system.
S14	Any damage to the drainage system would be rectified before the drainage system is completed to the satisfaction of the relevant authority.

Overland Flood Flow Paths

- 4.38. Overland flood flow paths would follow the natural topography of the land along the access road towards Sheppey Way.

Residual Risk

- 4.39. The proposed drainage measures would ensure that there is little or no residual risk of property flooding occurring during events well in excess of the minimum acceptable standard of protection for new property, which requires that no flooding of property should occur as a result of a one in 100 year storm event including an appropriate allowance for climate change.
- 4.40. For extreme events it is considered that the proposed development would intercept any uncontrolled overland flow and direct it into the proposed drainage system. The proposed drainage measures would ensure the proposed development would have adequate flood protection for extreme events over the lifetime of the development.

5. MAINTENANCE STRATEGY

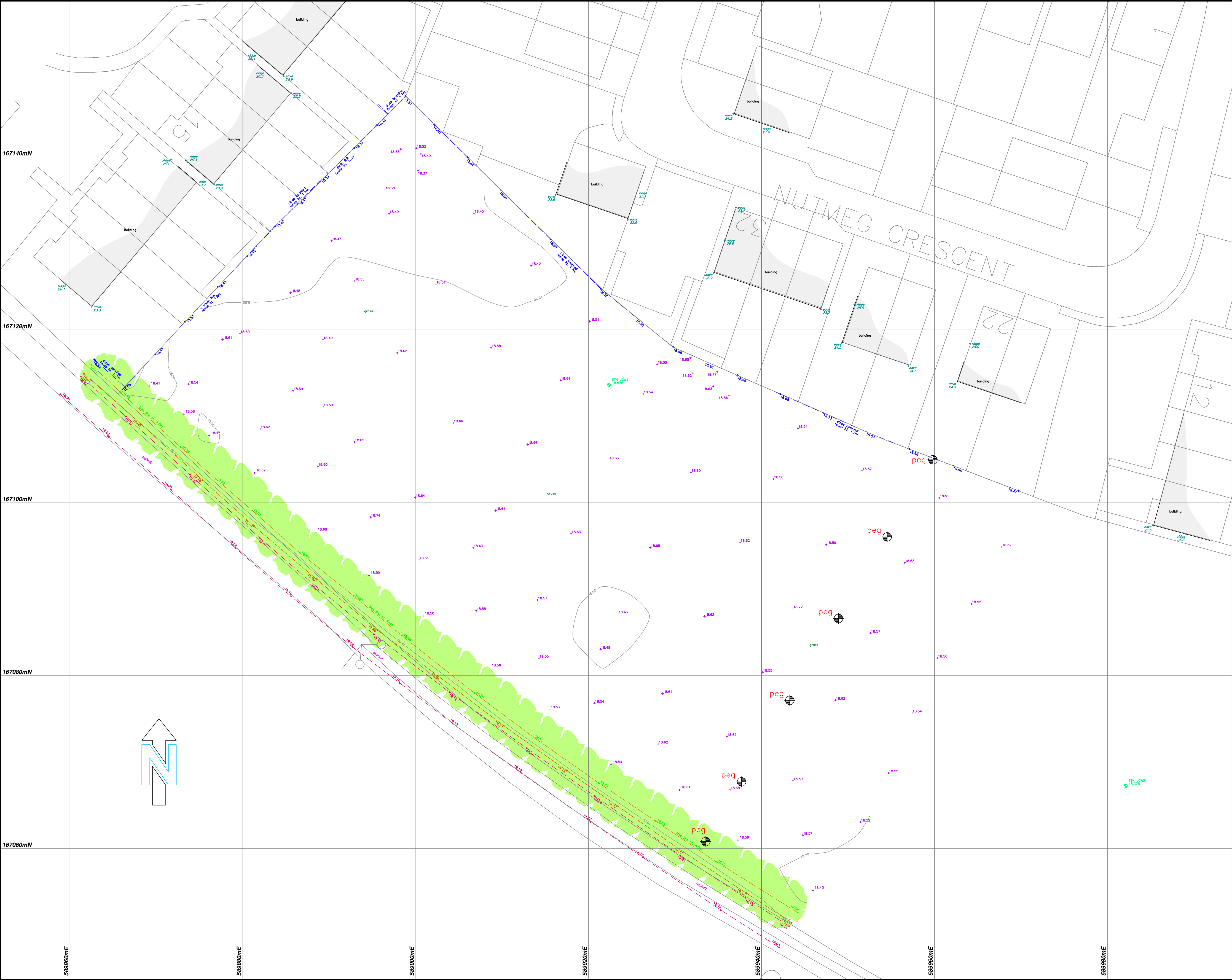
- 5.1. In terms of the maintenance strategy for the proposed drainage measures, the main surface drainage systems would be adopted by Southern Water, in its role as sewerage undertaker, under a Section 104 Agreement of the Water Industry Act 1991. Southern Water would therefore be responsible for the future maintenance of the adopted drainage systems
- 5.2. As Southern Water does not presently adopt surface water attenuation features it is proposed that any such feature (such as a geocellular tank) would be maintained by a Management Company.
- 5.3. Roads and footways, including highway drainage and gullies, to be adopted under Section 38 of the Highways Act 1980, would be maintained by Kent County Council in its role as local highway authority.
- 5.4. An outline Maintenance plan for the SuDS components in accordance with this guidance are set out in **Table D** below.

Table D: Operation and maintenance requirements SuDS Features

Maintenance Schedule	Required Action	Typical Frequency
Geocellular Tank		
Regular Maintenance	Inspect and identify any areas that are not operating correctly. If required take remedial action.	Monthly for 3 months, then annually
	Remove debris from the catchment surface (where it may cause risks to performance)	Monthly
	Remove sediment from pre-treatment structures and/or internal forebays	Annually, or as required.
Remedial actions	Repair/rehabilitate inlets, outlet, overflows and vents	As required
Monitoring	Inspect/check all inlets, outlets, vents and overflows to ensure that they are in good condition and operating as designed.	Annually
	Survey inside of tank for sediment build-up and remove if necessary	Every 5 years or as required.
Pervious Pavement		
Regular Maintenance	Brushings and vacuuming (standard cosmetic sweep over whole surface)	Once a year, after autumn leaf fall, or reduced frequency as required, based on site-specific observations of clogging or manufacturer's recommendations
Occasional maintenance	Removal of weeds or management using glyphosphate applied directly into the weeds by an applicator rather than spraying	As required – once per year on less frequently used pavements
Remedial actions	Remediate any landscaping which, through vegetation maintenance or soil slip, has been raised to within 50 mm of the level of the paving	As required
	Remedial work to any depressions, rutting and cracked or broken blocks considered detrimental to the structural performance or a hazard to users, and replace lost jointing material	As required
	Rehabilitation of surface and upper substructure by remedial sweeping	Every 10 to 15 years or as required (if infiltration performance is reduced due to significant clogging)
Monitoring	Initial inspection	Monthly for three months after installation
	Inspect for evidence of poor operation and/or weed growth – if required, take remedial action	Three-monthly, 48 h after large storms in first six months
	Inspect silt accumulation rates and establish appropriate brushing frequencies	Annually
	Monitor inspection chambers	Annually

6. CONCLUSIONS

- 6.1. This Surface Water Management Statement has been prepared in connection with proposals for comprise 14 retirement cottages for sheltered accommodation on land off Sheppey Way, Iwade.
- 6.2. The overall site comprises 0.38 hectares, and is located to the west of Sheppey Way to the south of the village of Iwade.
- 6.3. The British Geological Survey (BGS) geological mapping of the area shows the site is underlain by London Clay Formation bedrock and Head superficial deposits. The available evidence suggests the use of soakaways would not provide a suitable means of draining surface water runoff from development on the site.
- 6.4. It is therefore necessary to use flow balancing methods in order to store and attenuate surface water runoff to the greenfield runoff rates which in this instance is a minimum practicable controlled flow rate of 2 l/s.
- 6.5. No formal drainage features (ditches or sewers) are identified on the site. A discharge to the Iwade Stream is not achievable and discharge to the local sewer network to the north of the site is proposed. The required storage will be provided using oversized pipes and an underground geocellular tank. Outflow from the storage facilities is controlled by means of suitable vortex flow control device. Car parking bays will be formed of 'lined' pervious pavement as a means of a collection of rainfall / runoff and as Source Control.
- 6.6. Preliminary calculations have been undertaken for the design of oversized pipes and attenuation requirements using MicroDrainage software. These preliminary calculations demonstrate that a suitable means of drainage can be provided to drain the developed site in terms of surface water runoff in accordance with the guidance and standards laid down.
- 6.7. The proposed drainage strategy would ensure that surface water arising from the developed site would be managed in a sustainable manner to mimic the surface water flows arising from the site prior to the proposed development, while reducing the flood risk to the site itself and elsewhere, taking climate change into account.
- 6.8. The proposed development complies with the relevant standards of the Government's 'Non-statutory technical standards for sustainable drainage systems'.
- 6.9. A maintenance strategy for the proposed surface water drainage measures to serve the development has been set out in this document and can be covered by a suitably worded condition.
- 6.10. The overall conclusions drawn from this Surface Water Management Statement are that a suitable means of drainage can be provided to serve the proposed development in terms of the disposal of surface water runoff.



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LEGEND

SERVICES

AV AIR VENT
CAJB CABLE JUNCTION BOX
CATV CABLE TELEVISION COVER
CD CABLE DUCT
CIP CABLE INSPECTION POINT
EIC ELECTRIC INSPECTION COVER
EJB ELECTRIC JUNCTION BOX
EP ELECTRICITY POLE
ER EARTHING ROD
FH FIRE HYDRANT
GIC GAS INSPECTION COVER
GJB GAS JUNCTION BOX
GV GAS VENT
JB JUNCTION BOX
MK(E) SERVICE MARKER (ELECTRIC)
MK(G) SERVICE MARKER (GAS)
MK(W) SERVICE MARKER (WATER)
OHW OVERHEAD WIRE
SC(G) STOP COCK (GAS)
SC(W) STOP COCK (W)
STP SUPPORT FOR TELEPHONE POLE
SV STOP VALVE
TIC TELEPHONE INSPECTION COVER
TJB TELEPHONE JUNCTION BOX
TP TELEPHONE POLE
WIC WATER INSPECTION COVER
WM WATER METER

LEVEL

DPC DAMP PROOF COURSE
THL THRESHOLD LEVEL
T.O.C TOP OF CHIMNEY
T.O.W TOP OF WALL
WL WATER LEVEL

INTERNAL

CLG CEILING LEVEL
DHL DOOR HEAD LEVEL
FL FLOOR LEVEL
SCLG SUSPENDED CEILING LEVEL
US UNDERSIDE
USB UNDERSIDE OF BEAM
WGL WINDOW CILL LEVEL
WHL WINDOW HEAD LEVEL

FEATURES

B BOLLARD
BH BORE HOLE
BP BRICK PILLAR
BS BUS STOP
CPS CONCRETE PAVING SLABS
FB FLOWER BED
LB LITTER BIN
LC LIGHTING COLUMN
P POST
PB POST BOX
RNP ROAD NAME PLATE
RS ROAD SIGN
RW RETAINING WALL
SP SIGN POST
SU STEP(S) UP
TCS TELEPHONE CALL BOX
TH TRIAL HOLE
TS TREE STUMP

CONTROL

OSBM ORDNANCE SURVEY BENCH MARK
STN SURVEY STATION
TM TEMPORARY BENCH MARK

TREE (girth/spread/height/species/no. of boles)
 DIRECTION OF LEAN
 PHOTOGRAPH NUMBER, LOCATION & DIRECTION

GATE - GATES
 FENCE
 BUILDING
 OVER HEAD BUILDING LINE
 FACE OF WALL
 BACK OF RETAINING WALL
 LINE
 CHANGE OF SURFACE
 EDGE OF UNDERGROWTH

BANKING
 TOP OF BANK
 BOTTOM OF BANK
 KERB
 DROP KERB
 VERGE
 CONTOUR WITH VALUE
 OVER HEAD WIRE
 HEDGE/TREE LINE

FOR FUTURE SURVEY WORK OR SETTING OUT, J.C. WHITE GEOMATICS LIMITED QUOTED SURVEY CONTROL COORDINATES & LEVELS MUST BE USED. UNDER NO CIRCUMSTANCES SHOULD ANY OTHER SURVEYED POINTS ON THE DRAWING BE USED OTHER THAN AS A GROSS ERROR CHECK.

TREE GIRTHS AND SPREADS ARE QUOTED AS A MEAN SIZE, AND SHOWN TO SCALE. WHILST EVERY EFFORT IS MADE TO IDENTIFY TREE SPECIES AND GAUGE HEIGHTS, NO RESPONSIBILITY CAN BE TAKEN FOR THE ACCURACY OF THIS INFORMATION.

WHILST EVERY EFFORT IS MADE TO ENSURE THAT PIPE DIAMETERS, INVERT LEVELS AND DRAINAGE TYPES ARE CORRECT, THE ACCURACY OF THIS INFORMATION CANNOT BE GUARANTEED, AND IT IS STRONGLY RECOMMENDED THAT EXISTING INFORMATION IS CHECKED PRIOR TO THE COMMENCEMENT OF ANY DETAILED DESIGN AND CONSTRUCTION WORKS.

LEVELS AT KERB LINES ARE CHANNEL LEVELS.

ALL COORDINATES ARE BASED ON A LOCAL GRID CENTERED ON AN OS ACTIVE RINEX DERIVED COORDINATE FOR STN JCW1. ALL COORDINATES HAVE BEEN COMPUTED USING A SCALE FACTOR OF 1.00000.

DUE TO THE UNMAINTAINED NATURE OF THE SITE, IT CANNOT BE GUARANTEED THAT ALL FEATURES HAVE BEEN SURVEYED.

SURVEY LEVELS ADJUSTED TO FIT TO EXISTING "SURVEY SOLUTIONS" TOPOGRAPHICAL SURVEY DATED 30/07/2018.

LEVELS ARE BASED ON STATION ST03 (VALUE 18.321).

OS DATA SHOWN IN GREY.

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CONTROL SCHEDULE				
STATION	EASTING	NORTHING	HEIGHT	DESCRIPTION
JCW1	589922.337	167113.630	18.578	Peg
JCW2	589982.114	167067.255	18.375	Peg

A BOUNDARY SET-OUT PEGS ADDED [18/06/121]

REV. DESCRIPTION DATE INITIAL

03.06.19 PV

J. C. WHITE
Geomatics Limited
Shrine Barn, Shrine Farm, Sandling Road, Postling, Hythe, Kent, CT21 4HE
Tel : 01303 261212 Fax : 01303 264040
Email : survey@jcwhite.co.uk Web site : www.jcwhite.co.uk

• GPS Surveys
• Volumetric Surveys
• Topographical Surveys
• Measured Building Surveys
• Laser Scanning

• Setting Out
• Boundary Disputes
• Engineering Surveys
• Deformation & Settlement Surveys
• Scan to BIM Modelling

CLIENT
Middlefields Ltd.

JOB TITLE
Sheppy Way,
Iwade, Kent,
ME9 8TY.

DRAWING TITLE
Topographical
Survey

JOB No. 19/00/060 DATE March 2019

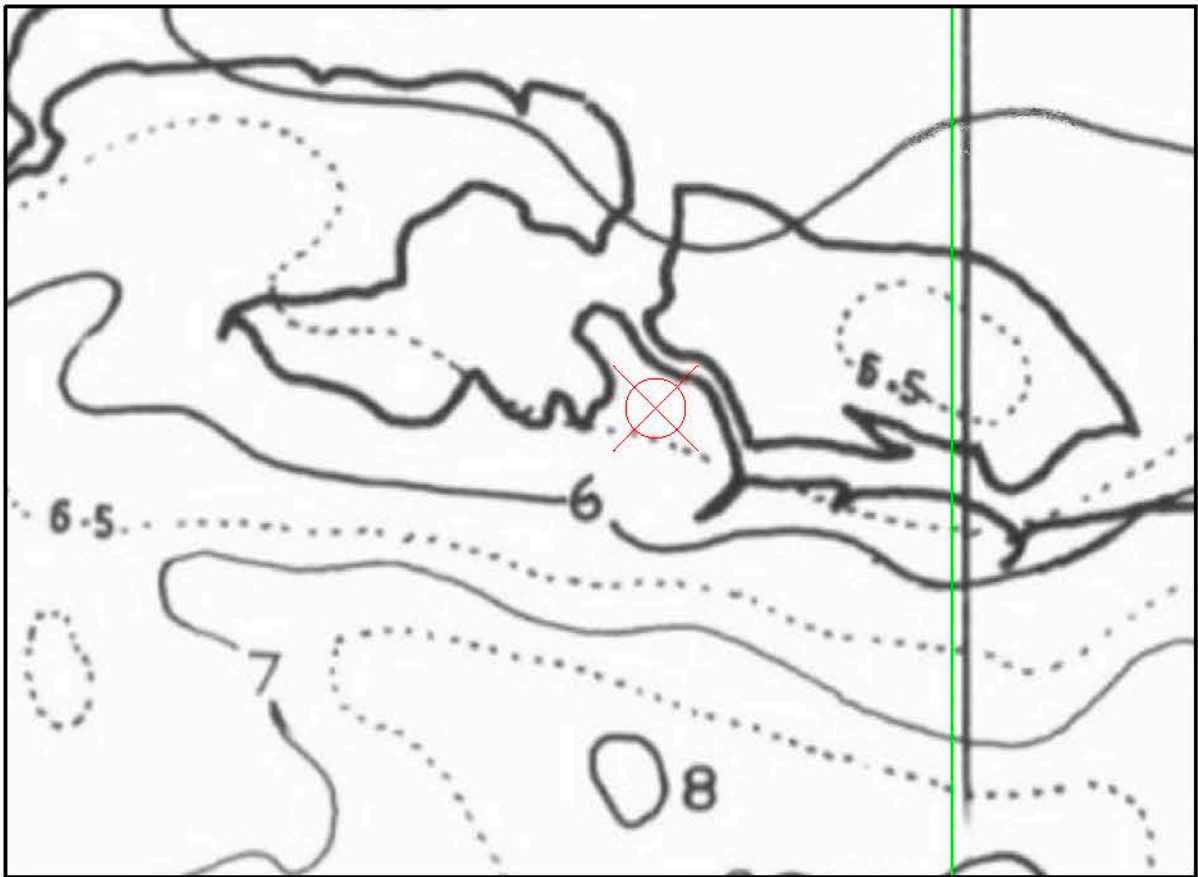
SURVEYED BY PV DRAWN BY PV

SCALE 1:200 DWG. No. 1 REV. No.

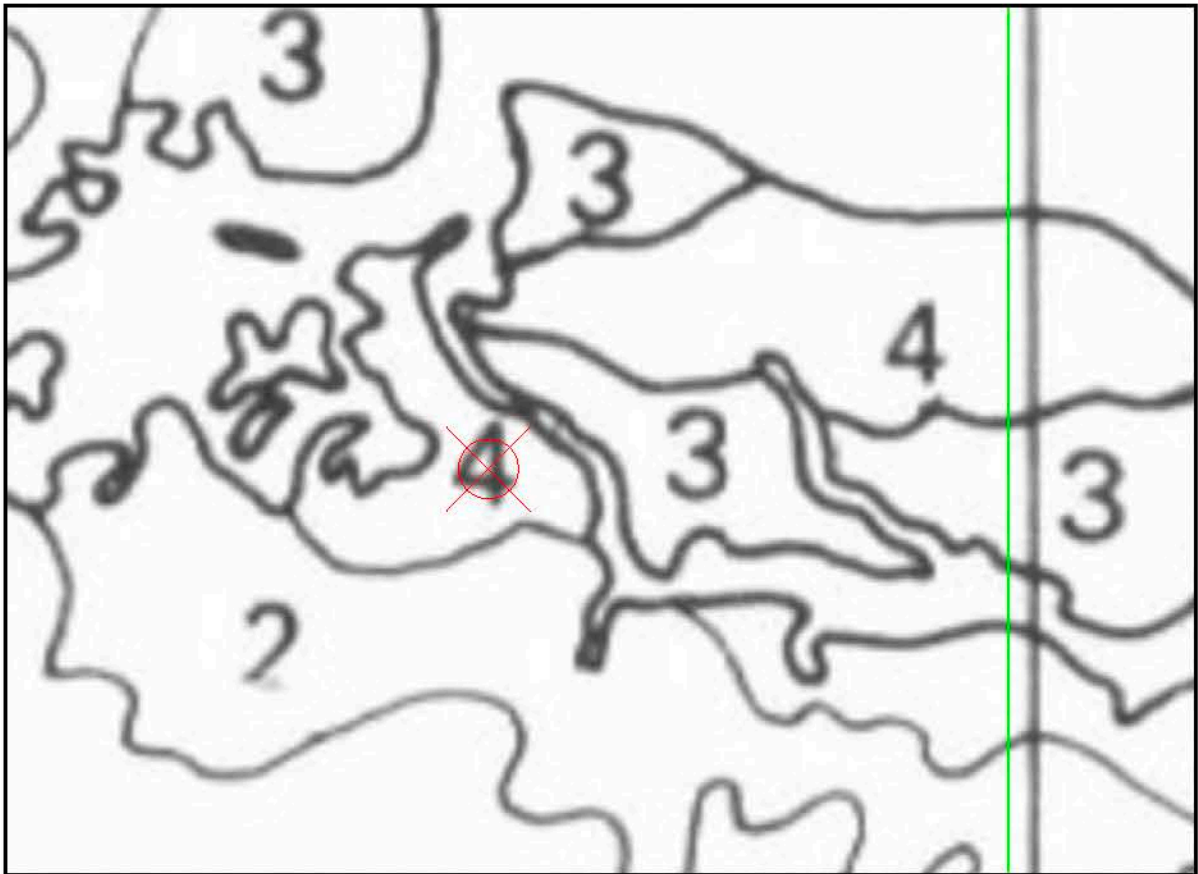
CAD PLOT DATE 11.09.2019 ORIGINAL SHEET SIZE A1 CADFILE NAME 19000060 - Iwade - Topographical Survey_REV_A.dwg



Location Plan



Standard Average Annual Rainfall (SAAR) (in hundreds of mm)



Winter Rain Acceptance Potential (WRAP)



Stratton Park House, Wanborough Road
Swindon, SN3 4HG
Telephone
01793 828000
Website
www.pfapl.com

For Planning
These drawings are produced for the purposes of
supporting a planning application and should not be
relied upon for tender, pricing, or construction purposes.

NOTES

1. Standard Average Annual Rainfall
(SAAR) and Winter Rain Acceptance
Potential (WRAP) map extracts shown
on this drawing are reproduced from
the maps contained in Volume V of
the Flood Studies Report –
NERC:1975.

Soil Classification				
Soil Class (WRAP)	Soil Index (LH)	SPR (FH)	SL (ADAS)	
1	0.15	10	0.1	
2	0.30	30	0.5	
3	0.40	37	0.8	
4	0.45	47	1.0	
5	0.50	53	1.3	

Rev	Date	Description	Drawn	Check
1	19.09.19	First Issue	BF	GL

Status
FOR PLANNING

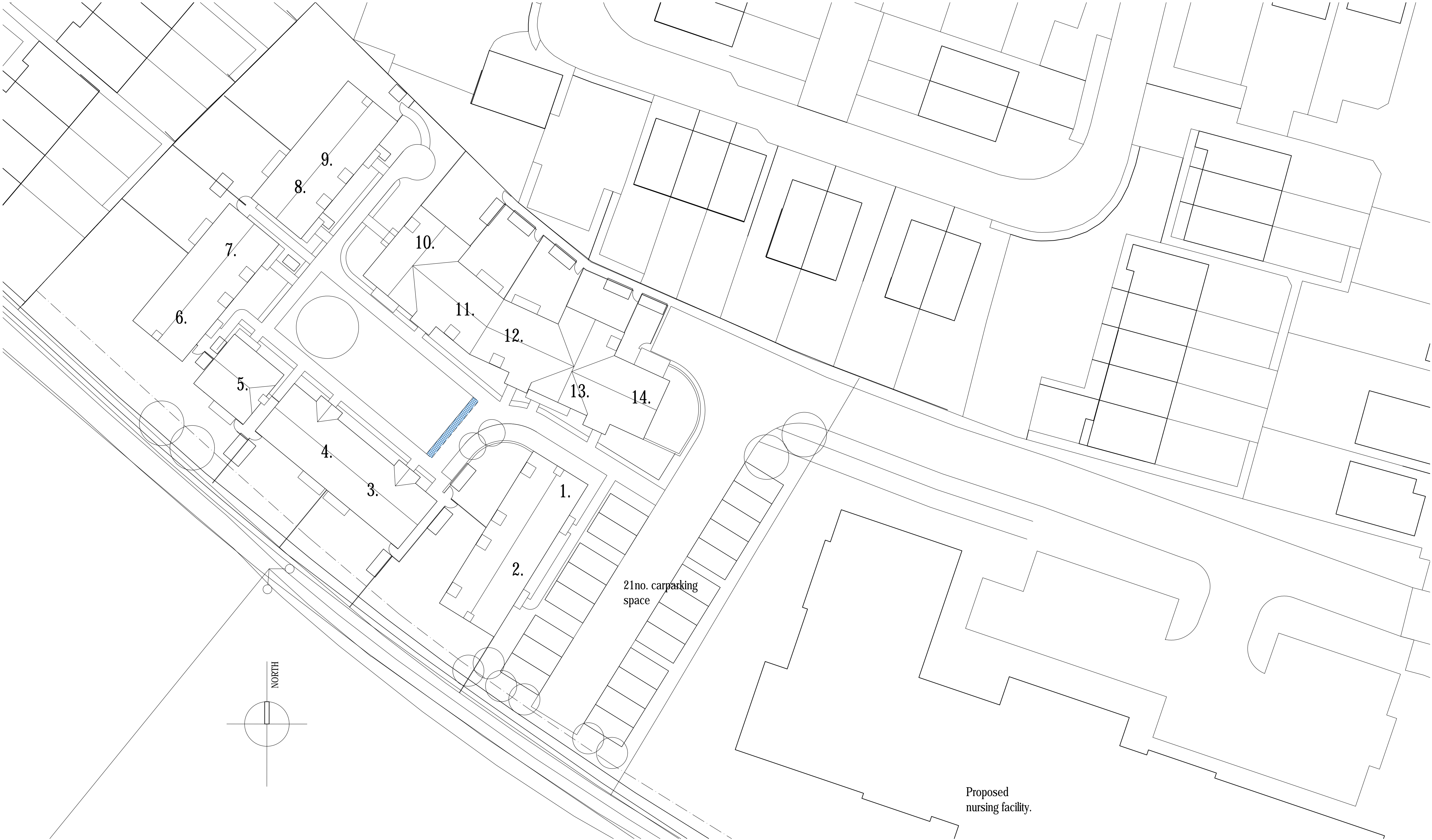
Client
Middlefields Ltd

Project
**Land at Sheppey Way,
Iwade**

Drawing Title
SAAR and WRAP Maps

Drawing No. **P912/01**

Date: September 2019 Scale: NTS
E-Mail: bfox@pfapl.com



Rev.	Description	Int.	Date

Client

HUME PLANNING

Job Title

PROPOSED RETIREMENT COTTAGES AT IWADE

CDP

CDP Architecture Ltd

22-23 North Lane, Canterbury

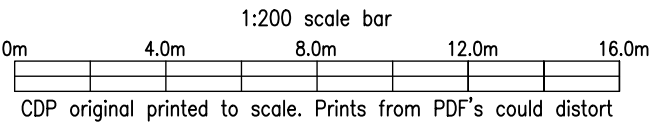
Kent, CT2 7EE

Tel: 01227 458181

Fax: 01227 451543

info@thinkcdp.com


www.thinkcdp.com




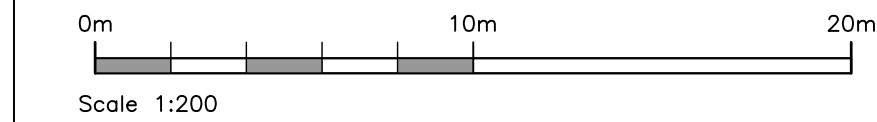
Drawing Title
PROPOSED
SITE PLAN

Scale @ A1	1:200	Preliminary/Comment
Drawn	MW	Planning
Date	AUG 2019	Building Regulations
Checked		Tender
		Construction
		As built

766	:	P02
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PFA Consulting		Page 1																								
Stratton Park House	P912																									
Wanborough Road	Land off Sheppey Way, ...																									
Swindon SN3 4HG	Greenfield run-off rate																									
Date 01/08/2019	Designed by AB																									
File	Checked by BF																									
Causeway		Source Control 2018.1.1																								
<p align="center"><u>ICP SUDS Mean Annual Flood</u></p> <p align="center">Input</p> <table> <tr> <td>Return Period (years)</td> <td>2</td> <td>Soil</td> <td>0.450</td> </tr> <tr> <td>Area (ha)</td> <td>1.000</td> <td>Urban</td> <td>0.000</td> </tr> <tr> <td>SAAR (mm)</td> <td>650</td> <td>Region Number</td> <td>Region 7</td> </tr> </table> <p align="center">Results 1/s</p> <table> <tr> <td>QBAR Rural</td> <td>4.0</td> </tr> <tr> <td>QBAR Urban</td> <td>4.0</td> </tr> <tr> <td>Q2 years</td> <td>3.5</td> </tr> <tr> <td>Q1 year</td> <td>3.4</td> </tr> <tr> <td>Q30 years</td> <td>9.1</td> </tr> <tr> <td>Q100 years</td> <td>12.9</td> </tr> </table>			Return Period (years)	2	Soil	0.450	Area (ha)	1.000	Urban	0.000	SAAR (mm)	650	Region Number	Region 7	QBAR Rural	4.0	QBAR Urban	4.0	Q2 years	3.5	Q1 year	3.4	Q30 years	9.1	Q100 years	12.9
Return Period (years)	2	Soil	0.450																							
Area (ha)	1.000	Urban	0.000																							
SAAR (mm)	650	Region Number	Region 7																							
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Q2 years	3.5																									
Q1 year	3.4																									
Q30 years	9.1																									
Q100 years	12.9																									
©1982-2018 Innovyze																										

PFA Consulting		Page 1
Stratton Park House	P912	
Wanborough Road	Land off Sheppey Way, ...	
Swindon SN3 4HG	Greenfield run-off	
Date 01/08/2019	Designed by AB	
File	Checked by BF	
Causeway		Source Control 2018.1.1
<p align="center"><u>ICP SUDS Mean Annual Flood</u></p> <p align="center">Input</p> <p>Return Period (years) 2 Soil 0.450</p> <p>Area (ha) 0.391 Urban 0.000</p> <p>SAAR (mm) 650 Region Number Region 7</p> <p align="center">Results 1/s</p> <p>QBAR Rural 1.6</p> <p>QBAR Urban 1.6</p> <p>Q2 years 1.4</p> <p>Q1 year 1.3</p> <p>Q30 years 3.6</p> <p>Q100 years 5.0</p>		
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Swindon, SN3 4HG

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KEY

- Site Boundary (Indicative Only)
- Proposed Surface Water Sewer
- Potential location for Attenuation Tank
- Proposed Lined Pervious Pavement
- Offsite Surface Water Sewer

NOTES

- Drawing is based on 'Proposed Site Plan' produced by CDP Architecture Ltd (Drawing No. 766 P02).
- Drawing is based on Topographical Survey produced by J. C. White (Drawing No. 19/00/060/1).
- Drainage is indicative only and is subject to detailed design and technical approval. Southern Water's asset data to be verified.

Rev	Date	Description	Drawn	Check
#	17/09/19	First Issue.	BF	GE

Status
FOR PLANNING


Client
Middlefields Ltd

Project
Land at Sheppey Way, Iwade

Drawing Title
Preliminary Surface Water Drainage Strategy

Drawing No.
P912/02













Date: September 2019 Scale: 1:200 @ A1
E-Mail: bfox@pfapl.com

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XP Solutions	Network 2019.1	

STORM SEWER DESIGN by the Modified Rational Method


Network Design Table for Storm

« - Indicates pipe capacity < flow

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)	Section Type	Auto Design
S1.000	26.030	0.174	149.6	0.061	5.00	0.0	0.600	o	150	Pipe/Conduit	
S1.001	4.819	0.028	172.1	0.038	0.00	0.0	0.600	o	225	Pipe/Conduit	
S1.002	20.123	0.118	170.5	0.000	0.00	0.0	0.600	o	225	Pipe/Conduit	
S2.000	22.284	0.045	495.2	0.053	5.00	0.0	0.600	o	900	Pipe/Conduit	
S1.003	16.024	0.032	500.8	0.012	0.00	0.0	0.600	o	900	Pipe/Conduit	
S1.004	26.730	0.178	150.2	0.018	0.00	0.0	0.600	o	150	Pipe/Conduit	
S1.005	5.465	0.036	151.8	0.000	0.00	0.0	0.600	o	150	Pipe/Conduit	
S3.000	13.430	0.090	150.0	0.000	5.00	0.0	0.600	o	150	Pipe/Conduit	
S1.006	12.264	0.082	149.6	0.000	0.00	0.0	0.600	o	150	Pipe/Conduit	
S1.007	24.722	0.182	135.8	0.000	0.00	0.0	0.600	o	150	Pipe/Conduit	
S1.008	20.736	0.123	168.6	0.000	0.00	0.0	0.600	o	225	Pipe/Conduit	
S1.009	20.820	0.104	200.2	0.000	0.00	0.0	0.600	o	375	Pipe/Conduit	

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
S1.000	87.02	5.53	17.651	0.061	0.0	0.0	0.0	0.82	14.5	14.3
S1.001	86.47	5.61	17.402	0.098	0.0	0.0	0.0	0.99	39.5	23.0
S1.002	84.25	5.95	17.374	0.098	0.0	0.0	0.0	1.00	39.7	23.0
S2.000	88.90	5.27	16.301	0.053	0.0	0.0	0.0	1.40	891.4	12.8
S1.003	83.04	6.14	16.256	0.164	0.0	0.0	0.0	1.39	886.4	36.8
S1.004	79.81	6.68	16.224	0.181	0.0	0.0	0.0	0.82	14.5«	39.2
S1.005	79.19	6.79	16.046	0.181	0.0	0.0	0.0	0.81	14.4«	39.2
S3.000	88.83	5.27	16.100	0.000	0.0	0.0	0.0	0.82	14.5	0.0
S1.006	77.83	7.04	16.010	0.181	0.0	0.0	0.0	0.82	14.5«	39.2
S1.007	75.37	7.52	15.850	0.181	0.0	0.0	0.0	0.86	15.2«	39.2
S1.008	73.71	7.87	15.593	0.181	0.0	0.0	0.0	1.00	39.9	39.2
S1.009	72.46	8.14	15.320	0.181	0.0	0.0	0.0	1.28	141.0	39.2

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Stratton Park House Wanborough Road Swindon SN3 4HG	P912: Land at Sheppey Way Iwade For Planning	
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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
S1.000	o	150	S1	18.664	17.651	0.863	Open Manhole	1200
S1.001	o	225	S2	18.667	17.402	1.040	Open Manhole	1200
S1.002	o	225	S3	18.696	17.374	1.097	Open Manhole	1200
S2.000	o	900	S4-Tank	18.701	16.301	1.500	Open Manhole	1800
S1.003	o	900	S5	18.642	16.256	1.486	Open Manhole	1800
S1.004	o	150	S6-CON	18.545	16.224	2.171	Open Manhole	1800
S1.005	o	150	S7	18.579	16.046	2.383	Open Manhole	1200
S3.000	o	150	SSW12	18.515	16.100	2.265	Open Manhole	1200
S1.006	o	150	S8	18.554	16.010	2.394	Open Manhole	1200
S1.007	o	150	S100	18.500	15.850	2.500	Open Manhole	1200
S1.008	o	225	S101	18.300	15.593	2.482	Open Manhole	1200
S1.009	o	375	S102	18.200	15.320	2.505	Open Manhole	1350


Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
S1.000	26.030	149.6	S2	18.667	17.477	1.040	Open Manhole	1200
S1.001	4.819	172.1	S3	18.696	17.374	1.097	Open Manhole	1200
S1.002	20.123	170.5	S5	18.642	17.256	1.161	Open Manhole	1800
S2.000	22.284	495.2	S5	18.642	16.256	1.486	Open Manhole	1800
S1.003	16.024	500.8	S6-CON	18.545	16.224	1.421	Open Manhole	1800
S1.004	26.730	150.2	S7	18.579	16.046	2.383	Open Manhole	1200
S1.005	5.465	151.8	S8	18.554	16.010	2.394	Open Manhole	1200
S3.000	13.430	150.0	S8	18.554	16.010	2.393	Open Manhole	1200
S1.006	12.264	149.6	S100	18.500	15.928	2.422	Open Manhole	1200
S1.007	24.722	135.8	S101	18.300	15.668	2.482	Open Manhole	1200
S1.008	20.736	168.6	S102	18.200	15.470	2.505	Open Manhole	1350
S1.009	20.820	200.2	SS104-TBC	18.100	15.216	2.509	Open Manhole	900

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XP Solutions		Network 2019.1


Area Summary for Storm

Pipe Number	PIMP Type	PIMP Name	PIMP (%)	Gross Area (ha)	Imp. Area (ha)	Pipe Total (ha)
1.000	User	-	100	0.013	0.013	0.013
	User	-	100	0.013	0.013	0.026
	User	-	100	0.010	0.010	0.036
	User	-	100	0.005	0.005	0.040
	User	-	100	0.005	0.005	0.046
	User	-	100	0.015	0.015	0.061
1.001	User	-	100	0.033	0.033	0.033
	User	-	100	0.005	0.005	0.038
1.002	-	-	100	0.000	0.000	0.000
2.000	User	-	100	0.015	0.015	0.015
	User	-	100	0.038	0.038	0.053
1.003	User	-	100	0.012	0.012	0.012
1.004	User	-	100	0.018	0.018	0.018
1.005	-	-	100	0.000	0.000	0.000
3.000	-	-	100	0.000	0.000	0.000
1.006	-	-	100	0.000	0.000	0.000
1.007	-	-	100	0.000	0.000	0.000
1.008	-	-	100	0.000	0.000	0.000
1.009	-	-	100	0.000	0.000	0.000
				Total	Total	Total
				0.181	0.181	0.181

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Free Flowing Outfall Details for Storm

Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)
S1.009	SS104-TBC	18.100	15.216	14.691	900	0

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XP Solutions	Network 2019.1	

Online Controls for Storm

Hydro-Brake® Optimum Manhole: S6-CON, DS/PN: S1.004, Volume (m³): 15.0

Unit Reference MD-SHE-0055-2000-2276-2000
Design Head (m) 2.276
Design Flow (l/s) 2.0
Flush-Flo™ Calculated
Objective Minimise upstream storage
Application Surface
Sump Available Yes
Diameter (mm) 55
Invert Level (m) 16.224
Minimum Outlet Pipe Diameter (mm) 75
Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (l/s)	Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	2.276	2.0	Kick-Flo®	0.493	1.0
Flush-Flo™	0.242	1.2	Mean Flow over Head Range	-	1.5

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated


Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	1.1	0.800	1.2	2.000	1.9	4.000	2.6	7.000	3.4
0.200	1.2	1.000	1.4	2.200	2.0	4.500	2.7	7.500	3.5
0.300	1.2	1.200	1.5	2.400	2.0	5.000	2.9	8.000	3.6
0.400	1.2	1.400	1.6	2.600	2.1	5.500	3.0	8.500	3.7
0.500	1.0	1.600	1.7	3.000	2.3	6.000	3.1	9.000	3.8
0.600	1.1	1.800	1.8	3.500	2.4	6.500	3.2	9.500	3.9

Storage Structures for Storm

Cellular Storage Manhole: S4-Tank, DS/PN: S2.000

Invert Level (m) 16.571 Safety Factor 2.0
Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.95
Infiltration Coefficient Side (m/hr) 0.00000

Depth (m)	Area (m²)	Inf. Area (m²)	Depth (m)	Area (m²)	Inf. Area (m²)	Depth (m)	Area (m²)	Inf. Area (m²)
0.000	86.4	0.0	1.230	86.4	0.0	1.231	0.0	0.0

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Stratton Park House Wanborough Road Swindon SN3 4HG	P912: Land at Sheppey Way Iwade For Planning	
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XP Solutions	Network 2019.1	

1 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000
 Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000
 Hot Start Level (mm) 0 Inlet Coefficient 0.800
 Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000
 Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0
 Number of Online Controls 1 Number of Storage Structures 1 Number of Real Time Controls 0

Synthetic Rainfall Details


Rainfall Model FSR M5-60 (mm) 19.600 Cv (Summer) 0.750
 Region England and Wales Ratio R 0.400 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 299.0
 Analysis Timestep 2.5 Second Increment (Extended)
 DTS Status OFF
 DVD Status ON
 Inertia Status ON

Profile(s) Summer and Winter
 Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440
 Return Period(s) (years) 1
 Climate Change (%) 0

PN	US/MH Name	Event	US/CL (m)	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow Vol (m³)	Maximum Vol (m³)
S1.000	S1	15 minute 1 year Winter I+0%	18.664	17.735	-0.066	0.000	0.59		0.090
S1.001	S2	15 minute 1 year Winter I+0%	18.667	17.506	-0.121	0.000	0.44		0.115
S1.002	S3	15 minute 1 year Winter I+0%	18.696	17.465	-0.134	0.000	0.34		0.135
S2.000	S4-Tank	120 minute 1 year Winter I+0%	18.701	16.648	-0.553	0.000	0.00		7.152
S1.003	S5	120 minute 1 year Winter I+0%	18.642	16.648	-0.508	0.000	0.01		4.757
S1.004	S6-CON	120 minute 1 year Winter I+0%	18.545	16.648	0.274	0.000	0.09		4.071
S1.005	S7	1440 minute 1 year Summer I+0%	18.579	16.078	-0.118	0.000	0.10		0.052
S3.000	SSW12	60 minute 1 year Winter I+0%	18.515	16.100	-0.150	0.000	0.00		0.000
S1.006	S8	1440 minute 1 year Summer I+0%	18.554	16.041	-0.119	0.000	0.09		0.059
S1.007	S100	1440 minute 1 year Summer I+0%	18.500	15.879	-0.121	0.000	0.08		0.028
S1.008	S101	1440 minute 1 year Summer I+0%	18.300	15.620	-0.198	0.000	0.03		0.025
S1.009	S102	1440 minute 1 year Summer I+0%	18.200	15.338	-0.357	0.000	0.01		0.019

PN	US/MH Name	Maximum Velocity (m/s)	Pipe Flow (l/s)	Status
S1.000	S1	0.8	8.1	OK
S1.001	S2	0.7	12.5	OK
S1.002	S3	0.8	12.4	OK
S2.000	S4-Tank	0.0	1.7	OK
S1.003	S5	0.1	3.1	OK
S1.004	S6-CON	0.5	1.2	SURCHARGED
S1.005	S7	0.4	1.2	OK
S3.000	SSW12	0.0	0.0	OK
S1.006	S8	0.5	1.2	OK
S1.007	S100	0.5	1.2	OK
S1.008	S101	0.5	1.2	OK
S1.009	S102	0.4	1.2	OK

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30 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000
 Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000
 Hot Start Level (mm) 0 Inlet Coefficient 0.800
 Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000
 Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0
 Number of Online Controls 1 Number of Storage Structures 1 Number of Real Time Controls 0

Synthetic Rainfall Details


Rainfall Model FEH Data Type Point
 FEH Rainfall Version 2013 Cv (Summer) 0.750
 Site Location GB 589960 167104 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 299.0
 Analysis Timestep 2.5 Second Increment (Extended)
 DTS Status OFF
 DVD Status ON
 Inertia Status ON

Profile(s) Summer and Winter
 Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440
 Return Period(s) (years) 30
 Climate Change (%) 0

PN	US/MH Name	Event	Water Surcharged Flooded						
			US/CL (m)	Level (m)	Depth (m)	Volume (m³)	Flow / Cap.	Overflow Vol (m³)	Maximum Vol (m³)
S1.000	S1	15 minute 30 year Winter I+0%	18.664	17.999	0.198	0.000	1.37		0.388
S1.001	S2	15 minute 30 year Summer I+0%	18.667	17.662	0.035	0.000	1.00		0.546
S1.002	S3	15 minute 30 year Winter I+0%	18.696	17.534	-0.065	0.000	0.83		0.263
S2.000	S4-Tank	360 minute 30 year Winter I+0%	18.701	16.990	-0.211	0.000	0.00		36.095
S1.003	S5	360 minute 30 year Winter I+0%	18.642	16.990	-0.166	0.000	0.00		11.694
S1.004	S6-CON	360 minute 30 year Winter I+0%	18.545	16.990	0.616	0.000	0.09		9.125
S1.005	S7	360 minute 30 year Winter I+0%	18.579	16.078	-0.118	0.000	0.10		0.052
S3.000	SSW12	60 minute 30 year Winter I+0%	18.515	16.100	-0.150	0.000	0.00		0.000
S1.006	S8	360 minute 30 year Winter I+0%	18.554	16.041	-0.119	0.000	0.09		0.059
S1.007	S100	360 minute 30 year Winter I+0%	18.500	15.879	-0.121	0.000	0.08		0.028
S1.008	S101	360 minute 30 year Winter I+0%	18.300	15.620	-0.198	0.000	0.03		0.025
S1.009	S102	360 minute 30 year Winter I+0%	18.200	15.338	-0.357	0.000	0.01		0.019

PN	US/MH Name	Maximum Pipe		Status
		Velocity (m/s)	Flow (l/s)	
S1.000	S1	1.1	18.9	SURCHARGED
S1.001	S2	0.8	28.5	SURCHARGED
S1.002	S3	1.0	29.8	OK
S2.000	S4-Tank	0.0	1.0	OK
S1.003	S5	0.1	2.0	OK
S1.004	S6-CON	0.5	1.2	SURCHARGED
S1.005	S7	0.4	1.2	OK
S3.000	SSW12	0.0	0.0	OK
S1.006	S8	0.5	1.2	OK
S1.007	S100	0.5	1.2	OK
S1.008	S101	0.5	1.2	OK
S1.009	S102	0.4	1.2	OK

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+0% Sensitivity 100 year Return Period
Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000
Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000
Hot Start Level (mm) 0 Inlet Coefficient 0.800
Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000
Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0
Number of Online Controls 1 Number of Storage Structures 1 Number of Real Time Controls 0

Synthetic Rainfall Details


Rainfall Model FEH Data Type Point
Return Period (years) 100 Cv (Summer) 0.750
FEH Rainfall Version 2013 Cv (Winter) 0.840
Site Location GB 589960 167104

Margin for Flood Risk Warning (mm) 299.0
Analysis Timestep 2.5 Second Increment (Extended)
DTS Status OFF
DVD Status ON
Inertia Status ON

Profile(s) Summer and Winter
Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440
Sensitivity flows(s) (%) 0, +20, +40


PN	US/MH Name	Event	Water Surcharged Flooded						
			US/CL (m)	Level (m)	Depth (m)	Volume (m ³)	Flow / Cap.	Overflow Vol (m ³)	Maximum Vol (m ³)
S1.000	S1	15 minute 100 year Winter Q+0%	18.664	18.226	0.425	0.000	1.74		0.645
S1.001	S2	15 minute 100 year Winter Q+0%	18.667	17.681	0.054	0.000	1.34		0.610
S1.002	S3	15 minute 100 year Winter Q+0%	18.696	17.605	0.006	0.000	1.06		0.383
S2.000	S4-Tank	480 minute 100 year Winter Q+0%	18.701	17.289	0.088	0.000	0.04		61.397
S1.003	S5	480 minute 100 year Winter Q+0%	18.642	17.302	0.146	0.000	0.02		15.701
S1.004	S6-CON	480 minute 100 year Winter Q+0%	18.545	17.310	0.936	0.000	0.10		11.758
S1.005	S7	480 minute 100 year Winter Q+0%	18.579	16.080	-0.116	0.000	0.12		0.056
S3.000	SSW12	60 minute 100 year Winter Q+0%	18.515	16.100	-0.150	0.000	0.00		0.000
S1.006	S8	480 minute 100 year Winter Q+0%	18.554	16.042	-0.118	0.000	0.11		0.063
S1.007	S100	480 minute 100 year Winter Q+0%	18.500	15.881	-0.119	0.000	0.10		0.030
S1.008	S101	480 minute 100 year Winter Q+0%	18.300	15.621	-0.197	0.000	0.04		0.027
S1.009	S102	480 minute 100 year Winter Q+0%	18.200	15.341	-0.354	0.000	0.01		0.023

PN	US/MH Name	Maximum Pipe		Status
		Velocity (m/s)	Flow (l/s)	
S1.000	S1	1.4	24.1	SURCHARGED
S1.001	S2	1.0	38.3	SURCHARGED
S1.002	S3	1.0	38.1	SURCHARGED
S2.000	S4-Tank	0.1	21.6	SURCHARGED
S1.003	S5	0.1	8.6	SURCHARGED
S1.004	S6-CON	0.5	1.4	SURCHARGED
S1.005	S7	0.5	1.4	OK
S3.000	SSW12	0.0	0.0	OK
S1.006	S8	0.5	1.4	OK
S1.007	S100	0.5	1.4	OK

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+0%% Sensitivity 100 year Return Period
Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Maximum Pipe		Status
		Velocity (m/s)	Flow (l/s)	
S1.008	S101	0.5	1.4	OK
S1.009	S102	0.5	1.4	OK

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+20% Sensitivity 100 year Return Period
Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000
Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000
Hot Start Level (mm) 0 Inlet Coefficient 0.800
Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000
Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0
Number of Online Controls 1 Number of Storage Structures 1 Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model FEH Data Type Point
Return Period (years) 100 Cv (Summer) 0.750
FEH Rainfall Version 2013 Cv (Winter) 0.840
Site Location GB 589960 167104


Margin for Flood Risk Warning (mm) 299.0
Analysis Timestep 2.5 Second Increment (Extended)
DTS Status OFF
DVD Status ON
Inertia Status ON

Profile(s) Summer and Winter
Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440
Sensitivity flows(s) (%) 0, +20, +40

Water Surcharged Flooded


PN	US/MH Name	Event	US/CL (m)	Level (m)	Depth (m)	Volume (m ³)	Flow / Cap.	Overflow Vol (m ³)	Maximum Vol (m ³)
S1.000	S1	15 minute 100 year Winter Q+20%	18.664	18.485	0.684	0.000	2.02		0.938
S1.001	S2	15 minute 100 year Winter Q+20%	18.667	17.757	0.130	0.000	1.56		0.796
S1.002	S3	15 minute 100 year Winter Q+20%	18.696	17.653	0.054	0.000	1.23		0.448
S2.000	S4-Tank	480 minute 100 year Winter Q+20%	18.701	17.549	0.348	0.000	0.05		83.408
S1.003	S5	480 minute 100 year Winter Q+20%	18.642	17.572	0.416	0.000	0.03		16.991
S1.004	S6-CON	480 minute 100 year Winter Q+20%	18.545	17.582	1.208	0.000	0.11		12.491
S1.005	S7	480 minute 100 year Winter Q+20%	18.579	16.082	-0.114	0.000	0.13		0.059
S3.000	SSW12	60 minute 100 year Winter Q+20%	18.515	16.100	-0.150	0.000	0.00		0.000
S1.006	S8	480 minute 100 year Winter Q+20%	18.554	16.044	-0.116	0.000	0.12		0.066
S1.007	S100	480 minute 100 year Winter Q+20%	18.500	15.882	-0.118	0.000	0.10		0.031
S1.008	S101	480 minute 100 year Winter Q+20%	18.300	15.622	-0.196	0.000	0.04		0.028
S1.009	S102	480 minute 100 year Winter Q+20%	18.200	15.343	-0.352	0.000	0.01		0.025

		Maximum Pipe		
PN	US/MH Name	Velocity (m/s)	Flow (l/s)	Status
S1.000	S1	1.6	27.9	FLOOD RISK
S1.001	S2	1.1	44.6	SURCHARGED
S1.002	S3	1.1	44.4	SURCHARGED
S2.000	S4-Tank	0.1	27.6	SURCHARGED
S1.003	S5	0.1	11.7	SURCHARGED
S1.004	S6-CON	0.5	1.5	SURCHARGED
S1.005	S7	0.5	1.5	OK
S3.000	SSW12	0.0	0.0	OK
S1.006	S8	0.5	1.5	OK
S1.007	S100	0.5	1.5	OK

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+20%% Sensitivity 100 year Return Period
Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Maximum Pipe		Status
		Velocity (m/s)	Flow (l/s)	
S1.008	S101	0.5	1.5	OK
S1.009	S102	0.5	1.5	OK

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+40% Sensitivity 100 year Return Period
Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 0.000
Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000
Hot Start Level (mm) 0 Inlet Coefficient 0.800
Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000
Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0
Number of Online Controls 1 Number of Storage Structures 1 Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model FEH Data Type Point
Return Period (years) 100 Cv (Summer) 0.750
FEH Rainfall Version 2013 Cv (Winter) 0.840
Site Location GB 589960 167104


Margin for Flood Risk Warning (mm) 299.0
Analysis Timestep 2.5 Second Increment (Extended)
DTS Status OFF
DVD Status ON
Inertia Status ON

Profile(s) Summer and Winter
Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440
Sensitivity flows(s) (%) 0, +20, +40

Water Surcharged Flooded

PN	US/MH Name	Event	US/CL (m)	Level (m)	Depth (m)	Volume (m³)	Flow / Cap.	Overflow Vol (m³)	Maximum Vol (m³)
S1.000	S1	15 minute 100 year Winter Q+40%	18.664	18.664	0.863	0.340	2.25		1.472
S1.001	S2	15 minute 100 year Winter Q+40%	18.667	17.838	0.211	0.000	1.78		0.926
S1.002	S3	960 minute 100 year Winter Q+40%	18.696	17.784	0.185	0.000	0.32		0.602
S2.000	S4-Tank	960 minute 100 year Winter Q+40%	18.701	17.835	0.634	0.000	0.06		104.878
S1.003	S5	960 minute 100 year Winter Q+40%	18.642	17.844	0.688	0.000	0.04		17.799
S1.004	S6-CON	960 minute 100 year Winter Q+40%	18.545	17.857	1.483	0.000	0.12		13.192
S1.005	S7	960 minute 100 year Winter Q+40%	18.579	16.083	-0.113	0.000	0.14		0.061
S3.000	SSW12	60 minute 100 year Winter Q+40%	18.515	16.100	-0.150	0.000	0.00		0.000
S1.006	S8	960 minute 100 year Winter Q+40%	18.554	16.045	-0.115	0.000	0.12		0.069
S1.007	S100	960 minute 100 year Winter Q+40%	18.500	15.883	-0.117	0.000	0.11		0.033
S1.008	S101	960 minute 100 year Winter Q+40%	18.300	15.624	-0.194	0.000	0.05		0.030
S1.009	S102	960 minute 100 year Winter Q+40%	18.200	15.344	-0.351	0.000	0.01		0.028

		Maximum Pipe		
PN	US/MH Name	Velocity (m/s)	Flow (l/s)	Status
S1.000	S1	1.8	31.1	FLOOD
S1.001	S2	1.3	50.8	SURCHARGED
S1.002	S3	0.7	11.3	SURCHARGED
S2.000	S4-Tank	0.1	32.1	SURCHARGED
S1.003	S5	0.1	18.8	SURCHARGED
S1.004	S6-CON	0.5	1.6	SURCHARGED
S1.005	S7	0.5	1.6	OK
S3.000	SSW12	0.0	0.0	OK
S1.006	S8	0.5	1.6	OK
S1.007	S100	0.6	1.6	OK

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+40%% Sensitivity 100 year Return Period
Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Maximum Pipe		Status
		Velocity (m/s)	Flow (l/s)	
S1.008	S101	0.5	1.6	OK
S1.009	S102	0.6	1.6	OK