

**AMENDED**

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**Flood Risk Assessment**

**for**

**Proposed Residential Development at  
Bentletts Scrap Yard  
Claygate Road  
Collier Street  
Kent**

**1129-1008**

**February 2016**

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**Proposed Residential Development  
Bentletts Scrap Yard  
Claygate Road  
Collier Street  
Kent**

**Flood Risk Assessment  
With Drainage Strategy Layout**

**February 2016**

<b>Prepared by</b>	<b>Reviewed by</b>
Ray Clark	Mark Dann



**Client: Wealden Homes**

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2. Definition of Flood Hazard
3. Probability
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7. Off-site Impacts
8. Residual Risks
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## 0 INTRODUCTION

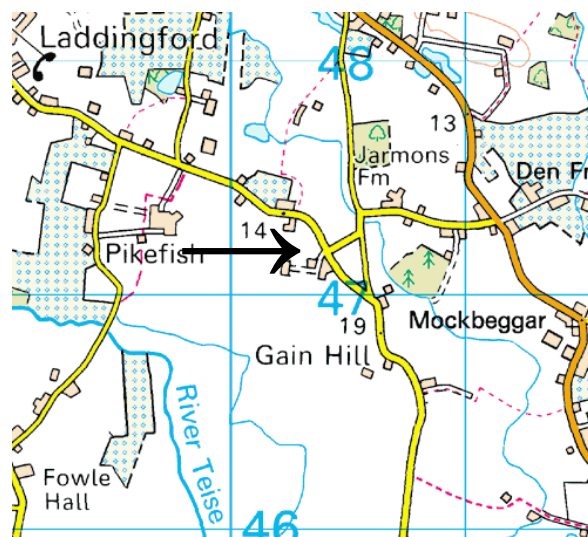
- a) Instructions were received from Wealden Homes to undertake a further Flood Risk Assessment to appraise a 25 dwelling development at Bentletts Scrap yard, Claygate Road, Collier Street, Kent. The previous assessment was for a 31 dwelling scheme.
- b) The assessment has been undertaken in compliance with the Technical Guidance to the National Planning Policy Framework March 2012 (NPPF).
- c) The information used for the preparation of this assessment is given in the Appendices.
- d) This assessment has been prepared by Ray Clark under guidance by RCD Consultants Ltd.
- e) The Client's attention is drawn to the Conditions and Limitations within Appendix F of this report.

## 1 DEVELOPMENT DESCRIPTION & LOCATION

### a) ***What type of development is proposed and where will it be located?***

The development site comprises the construction of 25 dwellings. The site is located at Bentletts Scrap Yard, Claygate Road, Collier Street, Kent.

### THE SITE



The site lies approximately 1Km from the nearest watercourse, River Teise, which is due southwest of the site. The subject site lies at approximately 50.5m AOD.

The existing site is classified as 'Brownfield' as it is an existing commercial vehicle scrap yard.

**b) *What is the vulnerability classification?***

In accordance with Table 2 in NPPF (March 2012), the proposed buildings are classified as “more vulnerable” being of residential use.

**c) *Is the proposed development consistent with the Local Development Documents?***

As far as Flood Risk is concerned the development is consistent with the Local Development Documents as it is located in Flood Zone 1, which is an area where **flooding does not occur**, refer to the Environment Agency mapping below and in the Appendices.

**d) *Please provide evidence that the Sequential Test or Exception Test has been applied in the selection of this site for this development type?***

The development is located within flood zone 1 and as identified in table 3 of the NPPF (March 2012) the development is appropriate for zone 1. The Sequential and Exception tests are therefore not required.

## 2 DEFINITION OF THE FLOOD HAZARD

### a) *What sources of flooding could affect the site?*

Potential Source	Yes/No
Flooding from Rivers	No
Flooding from the Sea	No
Flooding from Land	No
Flooding from Groundwater	No
Flooding from Sewers	No
Flooding from Reservoirs, Canals and other Artificial Sources	No

### b) *For each identified source, describe how flooding would occur, with reference to any historic records wherever these are available?*

#### FLOODING FROM RIVERS

The River Teise is approximately 1Km southwest of the proposed development.

The site lies on a ridge of land approximately 5-10m above surrounding levels associated with the River Teise. These surrounding areas are known to flood during extended rainfall events.

The Strategic Flood Risk Assessment, SFRA, confirms that there have been no reported instances of flooding from watercourses within the vicinity of the site.

The SFRA was prepared by Mott MacDonald in 2008.

The risk of flooding within the development boundaries, from Rivers, is considered to be low.

#### FLOODING FROM THE SEA

The site is not close to the sea and there have been no recorded instances of the site flooding due to the Sea.

#### FLOODING FROM LAND

The site lies on a ridge of high ground bounded by ditches and slopes towards Claygate Road.

It is therefore considered that the risk of flooding from the land is low.

#### FLOODING FROM GROUNDWATER

The risk of flooding from ground water is considered to be low as the underlying strata is impermeable Weald clay.

#### FLOODING FROM SEWERS

There are no public sewers within the vicinity of the site and all existing private sewers will be removed as part of the demolition process.

The risk of flooding from sewers is therefore low.

#### FLOODING FROM RESERVIORS, CANALS AND OTHER ARTIFICIAL SOURCES

The SFRA confirms that there have been no instances of flooding within the vicinity of the site.

**c) *What are the existing surface water drainage arrangements for this site?***

Surface water currently discharges to ditches adjacent to the site boundaries and as the site is predominantly hard standing this will be in the form of overland flows at an unrestricted rate during extreme storm events.

The existing hard standing areas have been measured at approximately 1.34Ha

The current owner has a trade effluent licence to discharge treated water to the ditches.

### 3 PROBABILITY

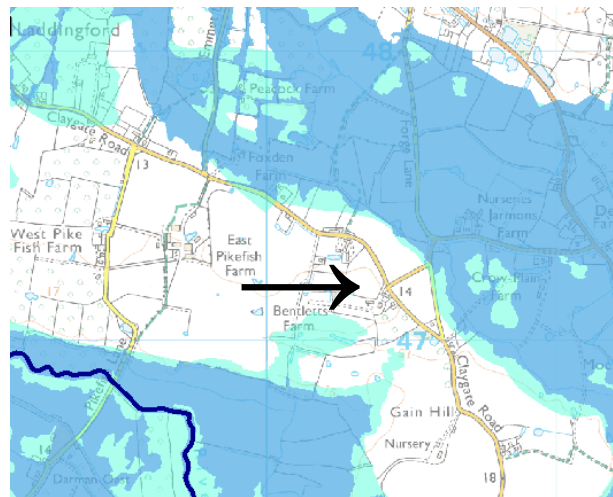
#### a) *Which flood zone is the site within?*

The relevant flood map attached to the SFRA which is included in the Appendix represents current best estimates of zone 2 and zone 3 flooding as defined in Table 1 of NPPF March 2012.

Zone 1	Low Probability of river or sea flooding
Zone 2	Medium Probability of river or sea flooding
Zone 3a	High Probability of river or sea flooding
Zone 3b	Functional Floodplain

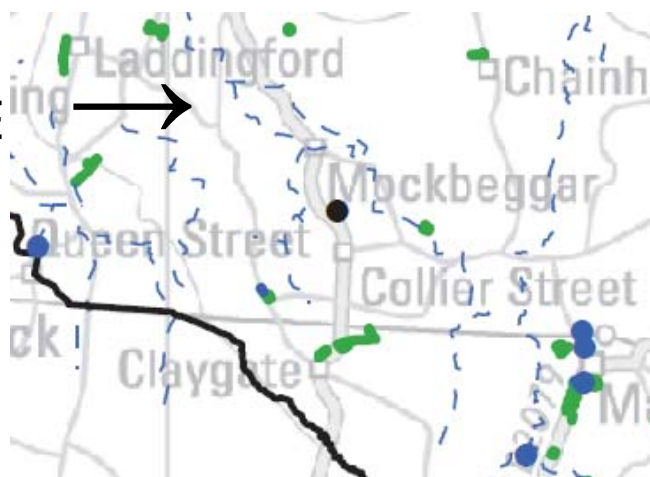
The map contained within the SFRA (extracts below) confirms that the site falls within Zone 1. A full copy of the map is included in Appendix A.

THE SITE



Extract from EA website showing risk of flooding from rivers

THE SITE



Extract from SFRA Map – Flood Risk Problems



b) ***If there is a Strategic Flood Risk Assessment covering this site, what does it show?***

A SFRA has been prepared by Mott MacDonald and Maidstone Borough Council and is dated May 2008. This shows that the site lies with Flood Zone 1 and is at a low risk of flooding.

c) ***What is the probability of the site flooding taking account of the contents of the SFRA and of any further site-specific assessments?***

The SFRA confirms that the site is located in Zone 1.

There will be a **decrease in runoff** from the site and this will be attenuated to a flow rate of 5.1l/s for the worst case 1 in 100 year storm event and will discharge to the stream on the northern boundary of the site.

The proposed drainage system will be designed to take account of a 30% climate change.

The residual risk of flooding is considered to be low.

d) ***What are the existing rates and volumes of run-off generated by this site?***

The site is currently Brownfield. Estimated flow rates (including an increase in rainfall intensity of 30%) are given in the following table:

Storm Return Period	Existing Flow Rate	Proposed Flow Rate (30% CC)
2 year	169.7l/s	5.0
30 years	327.5l/s	5.0
100 years	452.5l/s	5.1

Estimated volumes are as follows for storms of 6 hour duration (including an increase in rainfall intensity of 30% for the proposed development).

Storm Return Period	Existing Volume	Proposed Volume
2 year	319.1m <sup>3</sup>	96.2m <sup>3</sup>
30 years	573.6m <sup>3</sup>	172.9m <sup>3</sup>
100 years	741.2m <sup>3</sup>	223.5m <sup>3</sup>

**4 CLIMATE CHANGE**

**a) *How is flood risk at the site likely to be affected by climate change?***

The proposed development is for residential use and can be categorised to a 60yr design life.

In accordance with table 5 of NPPF March 2012 a 30% increase in peak rainfall intensity has been included in the development design calculations.

## 5 DETAILED DEVELOPMENT PROPOSALS

a) ***Please provide details of the development layout, referring to the relevant drawings.***

The proposed redevelopment comprises 25 dwellings with an impermeable area of 4040m<sup>2</sup>.

The drives will be constructed in porous paved materials to mimic Greenfield conditions.

The access road will also be constructed in porous paving but will be connected to the main drainage system to act as surface water attenuation during the worst case 1 in 100 year storm event.

A balancing pond will be incorporated into the design to provide additional surface water attenuation

A site drainage strategy layout is provided in Appendix C.

The flood receptors for the proposed development are the Residential Units.

The proposed development is classified as more vulnerable to table 2 of NPPF March 2012.

With regard to the proposed drainage strategy there is a preference to dispose of surface water run by infiltration methods. If infiltration is not possible then discharging to a watercourse should be considered before discharge to a sewer. The following table considers each of the options:

Method	Yes/No	Reason
Infiltration	No	Investigations show that the soils beneath the site are not capable of supporting an infiltration system.
Watercourse	Yes	There are ditches within the vicinity of the site
Sewers	No	There are no public surface water sewers within the vicinity of the site

The surface water generated by the roofs will be attenuated in line with NPPF March 2012 and discharge will be restricted to 5.1l/s for the worst case 1 in 100 year storm event. Attenuation will be in the form of ponds, porous paving and large diameter sewers up to 600mm.

Discharge of surface water will be to the ditch running along the northern boundary of the site

b) ***Where appropriate, demonstrate how land uses most sensitive to flood damage have been placed in areas within the site that are at least risk of flooding.***

The entire site is located in area of low flood risk.

## 6 FLOOD RISK MANAGEMENT MEASURES

- a) ***How will the site be protected from flooding, including the potential impacts of climate change, over the developments lifetime?***

The site is located in Zone 1 and is not at risk of flooding and flood risk management measures are not required. The design of the proposed drainage system will include a 30% increase in rainfall intensity to allow for the effects of climate change over the design life of the buildings.

## 7 OFF SITE IMPACTS

- a) ***How will you ensure that your proposed development and the measures to protect your site from flooding will not increase flood risk elsewhere?***

The existing scrapyards site has an approximate impermeable area of 1.34Ha and this will be reduced to 0.404Ha.

The proposed drainage will discharge to the ditch at a restricted rate of 5.1l/s for the worst case 1 in 100 year storm event.

The attenuation system will be designed to cater for a climate change allowance of 30%.

The surface water calculations shown in Appendix D and E show that both flow rate and volume of water entering the ditch will be significantly reduced as a result of the proposed development.

The risk of flooding elsewhere will therefore decrease as a result of the proposed development.

- b) ***How will you prevent run-off from the completed development causing an impact elsewhere?***

The surface water will be restricted to 5.1l/s for the worst case 1 in 100 year storm event and the design/calculations will include a 30% Climate Change allowance.

This is considerably lower than the prevailing existing conditions, estimated to be 452.5l/s for the worst case 1 in 100 year storm event.

The 741.2m<sup>3</sup> volume of pre-development surface water runoff will be reduced to 223.5m<sup>3</sup> as a result of the new development thus providing an additional capacity of 517.7m<sup>3</sup> within the downstream watercourse.

**8 RESIDUAL RISKS**

- a) ***What flood-related risks will remain after you have implemented the measures to protect the site from flooding?***

The drainage system will require periodic maintenance the details of which should be included in the overall building management plan to be handed over to the appointed management company.

- b) ***How and by whom will these risks be managed over the lifetime of the development?***

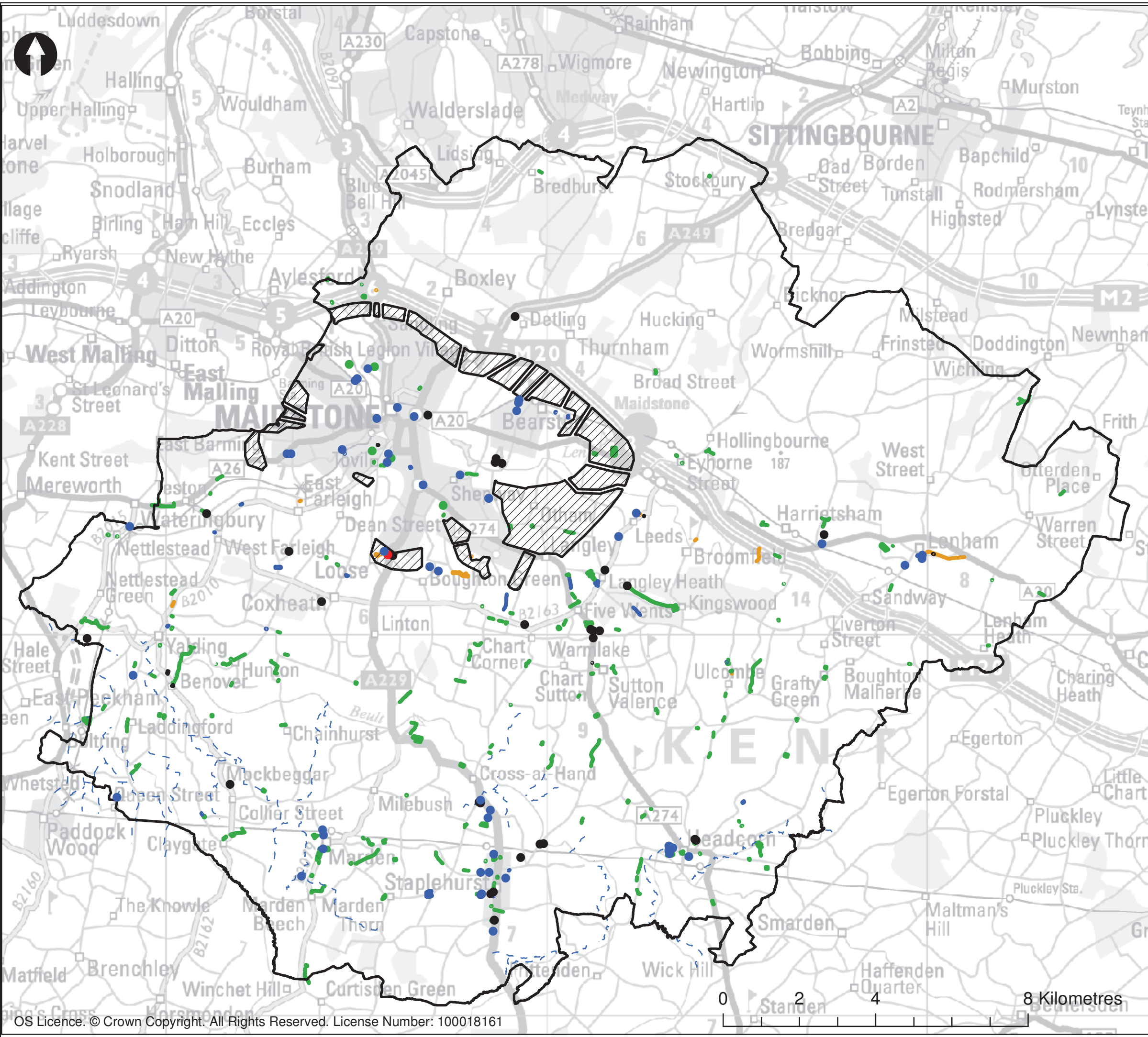
A management company will be appointed to ensure that the open spaces, ditches and ponds are maintained to ensure storage volume is not compromised within the attenuation system.

## 9 **CONCLUSIONS**

- The site currently drains treated surface water under a trade effluent licence to ditches at the site boundaries.
- The proposed development is located in Zone 1 and is at low risk of flooding.
- The redevelopment will bring about a considerable reduction in surface water discharge due to the decrease in impermeable area of the site and this will reduce any flooding impact elsewhere.
- All hardstandings will be constructed in porous paving materials to mimic Greenfield conditions.
- Roof drainage will discharge to an attenuation system and shall be restricted to 5.1l/s for the worst case 1 in 100 year storm event.
- Water quality from the proposed development will be considerably higher than existing because the porous paving will filter silt and contaminants. Currently the majority of the site is allowed to discharge to the stream unchecked and without any treatment.
- The porous paving of the new development is a recognised construction technique for the removal of spilled hydrocarbons before surface water discharge to the watercourses, hence no petrol interceptor will be required.
- The discharge of treated foul water will require an environmental permit from the Environment Agency.

**APPENDIX A:**

Flood Risk Map (from SFRA)  
Flooding Hotspot map (from SFRA)



**Legend**

- EA Main Rivers
- IDB Drains
- Maidstone Borough Boundary
- Area of Search

**Source of Flooding**

- Sewer Flooding
- Surface Water Flooding
- Groundwater Flooding
- Unknown Source

Scale 1:95,000

**Maidstone Borough SFRA**

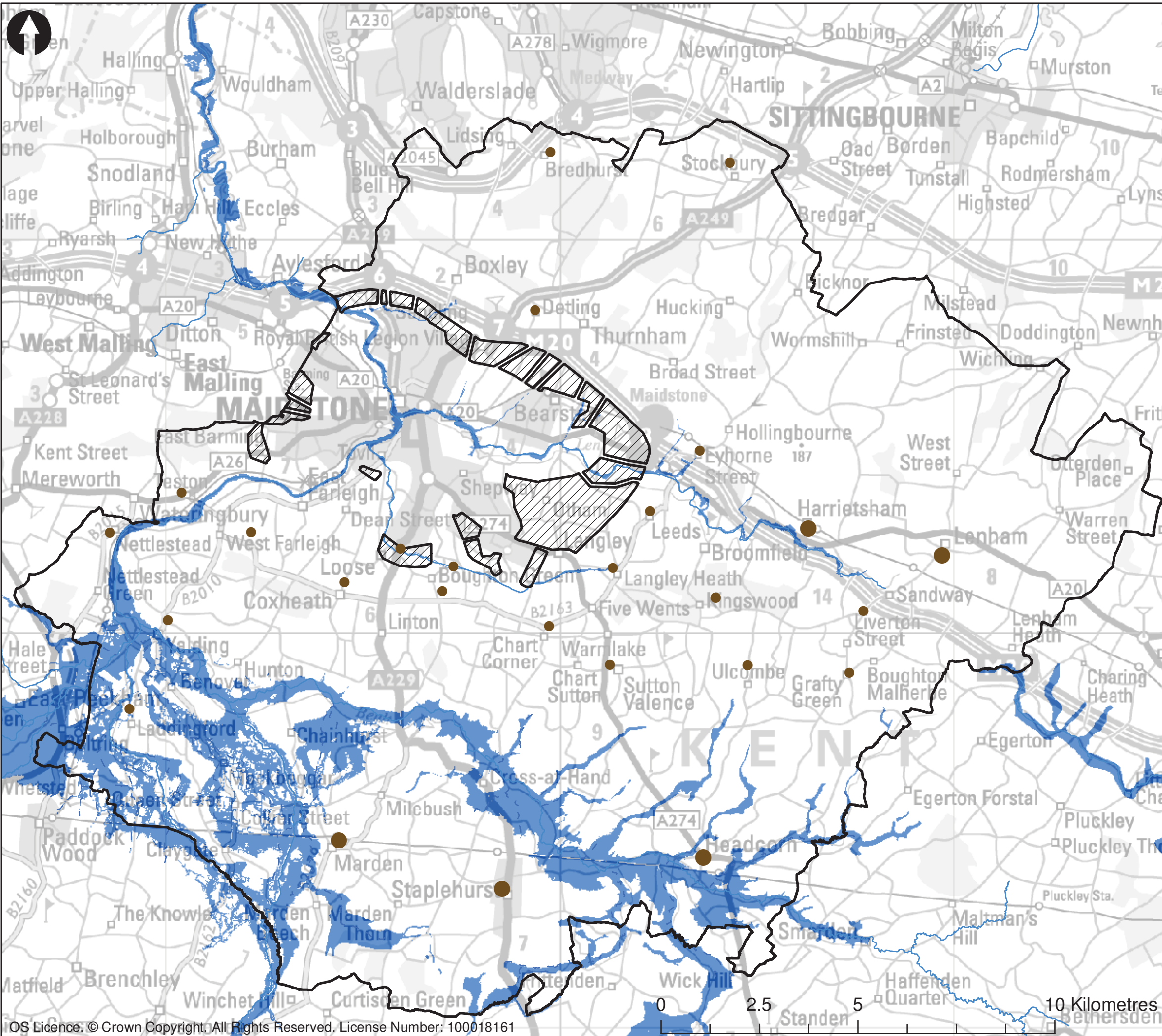
**Figure 4.1  
Reported Flood Incidents**

**May 2008**

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**Legend**

- EA Main Rivers —
- IDB Drains - - -
- Maidstone Borough Boundary □
- Area of Search ▨
- Rural Service Centre ●
- Larger Rural Settlement ●
- 1 in 100-year Flood Extent ■

Scale 1:95,000

**Maidstone Borough  
SFRA**

**Figure 5.2  
1 in 100 year Flood Extent  
(Flood Zone 3a)**

May 2008

**APPENDIX B:**

Topographical Survey

SURVEY STATIONS			
Name	Easting	Northing	Height
1	1000.000	2000.000	50.000
2	982.808	1994.258	50.103
3	973.095	1998.545	50.053
4	1000.043	2020.191	49.819
5	988.838	1938.519	50.238
6	998.798	2001.491	50.108
7	980.080	1918.054	49.883
8	987.843	1950.892	50.152
9	982.180	1925.178	50.191
10	946.400	1918.571	50.388
11	931.314	1918.320	50.489
12	914.980	1923.877	50.387
13	887.183	1923.247	50.423
14	857.878	1928.802	50.728
15	788.883	1954.089	50.718
16	753.054	1945.127	50.638
17	737.482	1954.888	50.824
18	808.323	1950.214	50.811
19	843.328	1958.781	50.728
20	878.738	1962.547	50.823
21	948.708	1978.072	49.847
22	924.873	2028.832	49.889

LEGEND

BOUNDARY	---	BOUNDARY	---
ROAD	---	ROAD	---
RAIL	---	RAIL	---
WATER	---	WATER	---
...	...	...	...

TREE LEGEND

...	...	...	...
...	...	...	...
...	...	...	...

FENCE DESCRIPTIONS

...	...	...	...
...	...	...	...

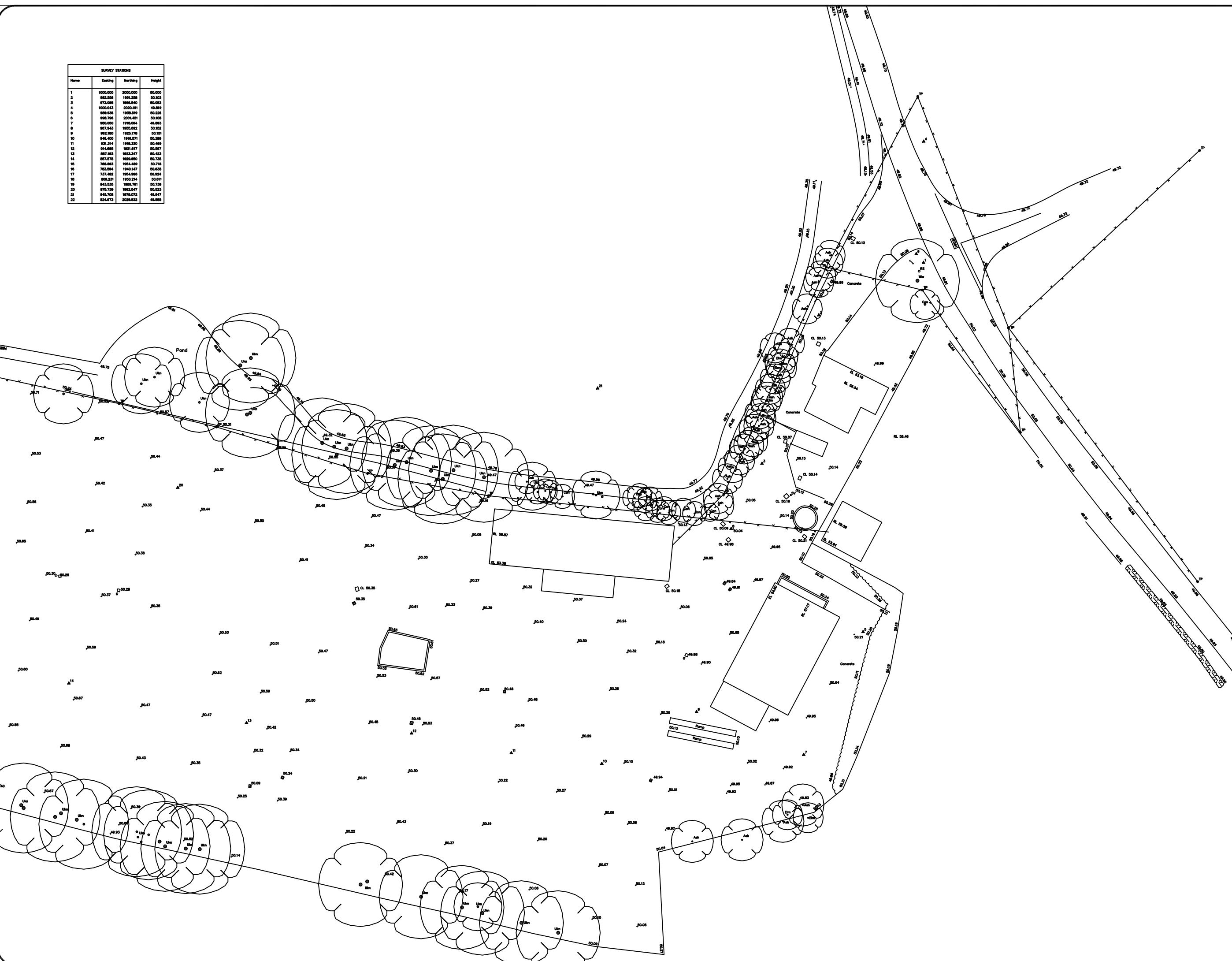
Bentletts Yard  
Laddingford

Site Survey

Date	1:200	Drawn By	T.S.
Date	Feb '14	Checked By	B.S.
Drawing No.	BYL/1260/1 of 2		

NOTES

1. TREES - The trees shown have been identified to the best of the surveyors knowledge, with the most correct drawn to scale. Tree heights are approximate.
2. DRAINAGE - All drainage has been surveyed by visual inspection only and should be cross checked in critical areas.
3. FENCES - Fences shown are not necessarily legal boundaries.
4. GRID - The survey grid is based on arbitrary co-ordinates. Not Ordnance Survey.



SURVEY STATIONS			
Name	Easting	Northing	Height
1	1000.000	2000.000	50.000
2	982.258	1991.258	50.103
3	973.085	1986.540	50.563
4	1000.043	2030.191	48.819
5	986.829	1928.919	50.238
6	996.796	2007.491	50.128
7	980.050	1918.084	49.883
8	987.843	1906.692	50.182
9	985.180	1925.178	50.181
10	948.400	1918.271	50.388
11	891.314	1918.320	50.489
12	914.698	1921.617	50.887
13	887.183	1923.247	50.423
14	897.078	1928.890	50.739
15	788.863	1954.498	52.718
16	783.884	1940.147	50.638
17	727.482	1904.898	50.804
18	808.291	1922.214	50.811
19	843.835	1898.781	50.739
20	878.729	1902.647	50.823
21	945.708	1979.072	48.847
22	824.873	2028.832	48.888

LEGEND

**BOUNDARY**  
 CHAIN OF MEASUREMENT (dashed line)  
 FENCE (line with cross-ticks)  
 TREE (circle with cross-hairs)  
 POLE (circle with cross)  
 WALL (line with cross-ticks)  
 LEVEL (triangle with number)  
 DRIVEWAY (rectangle with diagonal lines)

**ROADS**  
 DRIVE (solid line)  
 ROAD (double solid line)  
 RAILWAY (line with cross-ticks and wavy line)

**BUILDINGS**  
 RECTANGLE (solid line)

**OTHER**  
 POND (cloud-like shape)

TREE LEGEND

**Species:** BEECH, BIRCH, HEDERA, HORNBEAM, LIME, LARCH, SASSAPARILLA, SPINNEY DOGWOOD, YEW  
**Flame:** FLAME  
**Other:** BROAD LEAVED, CONIFER, DEcidUOUS, EVERGREEN, FOLIAGE, FOLIAGE, FOLIAGE, FOLIAGE

FENCE DESCRIPTIONS

**Types:** BRICK, CONCRETE, METAL, WOODEN POST AND RAIL, WIRE, TRENCH

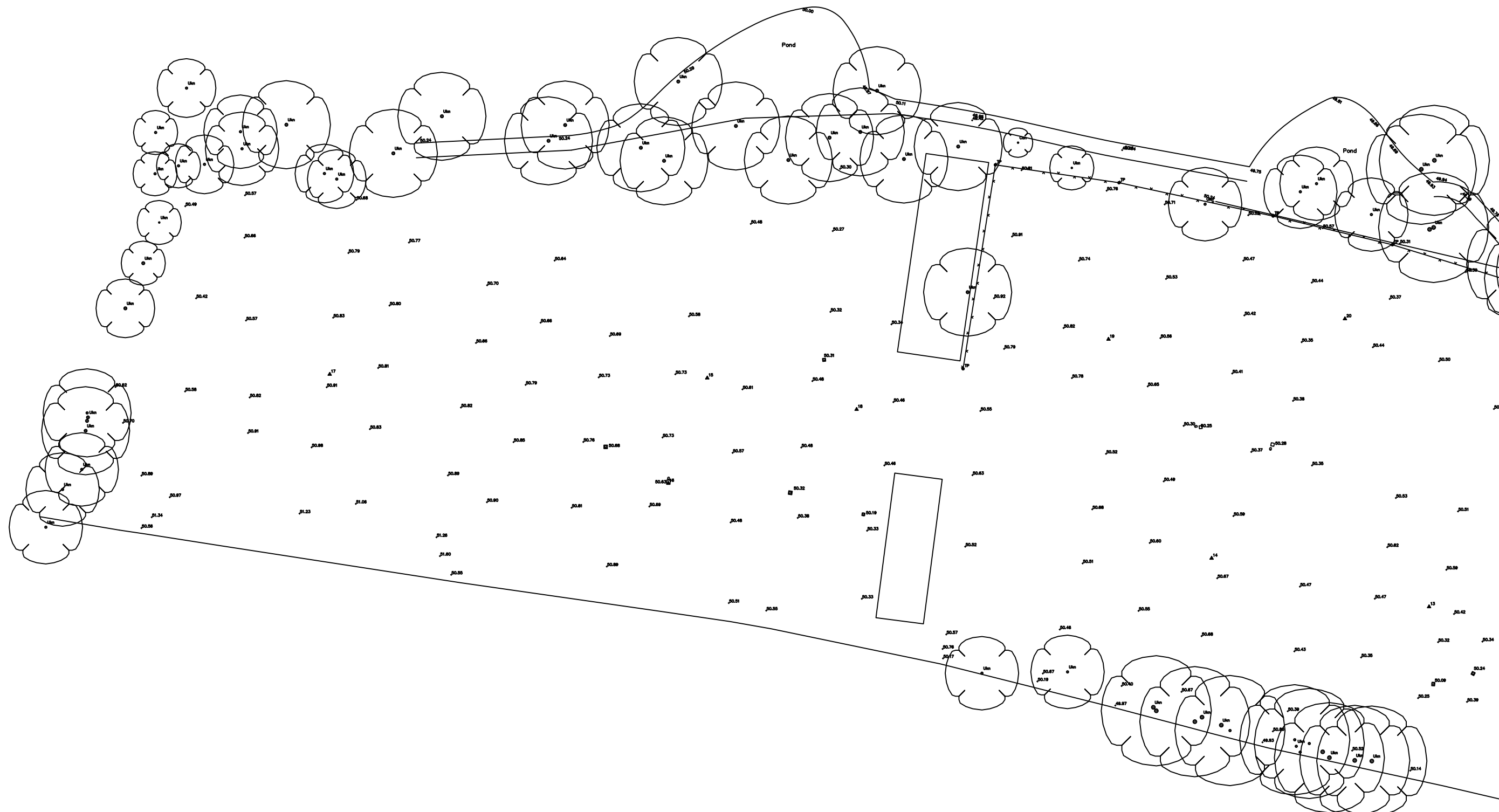
Bentletts Yard  
Laddingford

Site Survey

Scale: 1:200  
 Date: Feb '14  
 Drawn by: BYL/1260/2 of 2

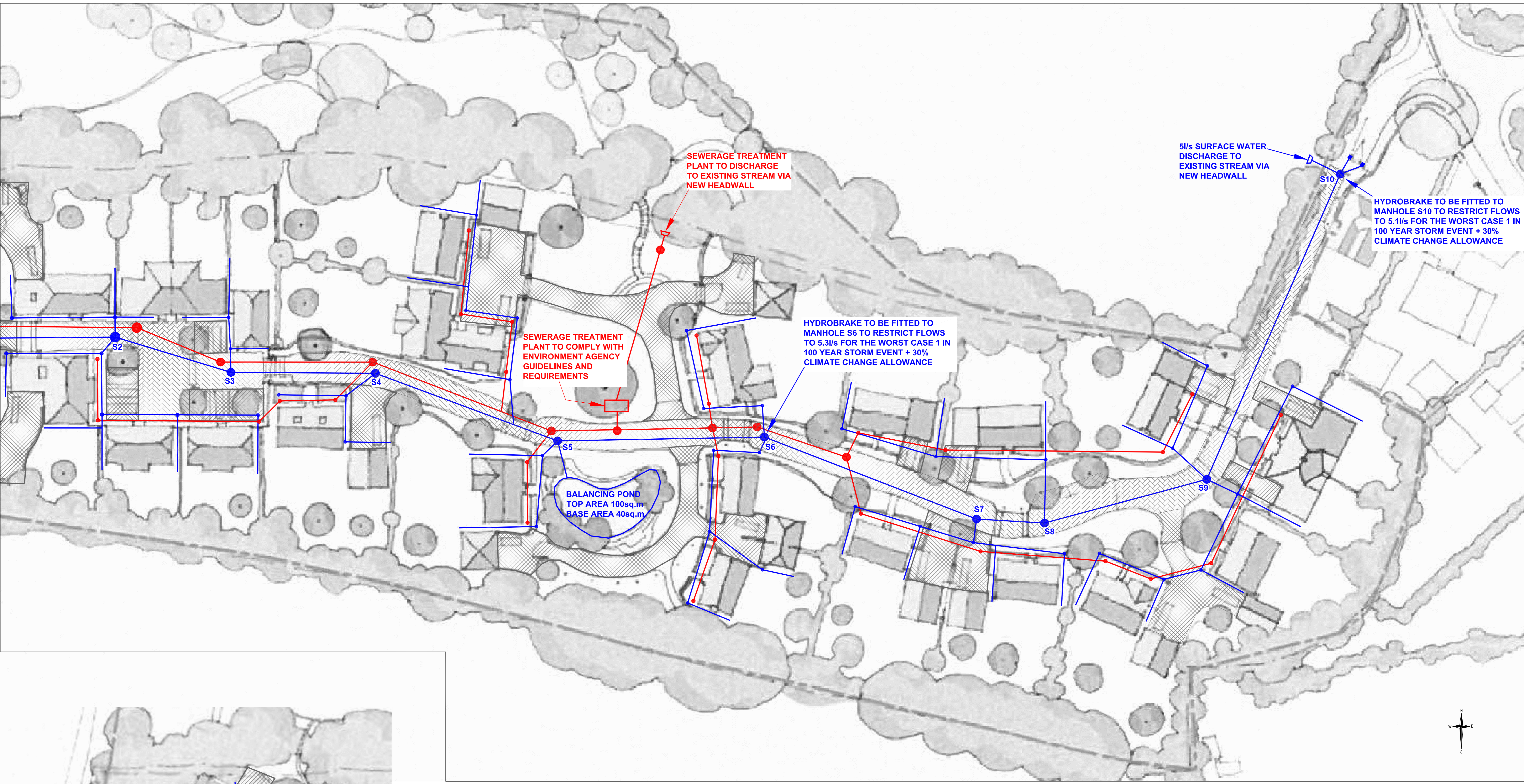
NOTES

- TREES - The tree species have been identified to the best of the surveyor's knowledge, with the main species shown to scale. Tree heights are approximate.
- DRAINAGE - All drainage has been surveyed by visual inspection only and should be cross checked in critical areas.
- FENCES - Fences shown **SHOULD** necessarily legal boundaries.
- LEVELS - The approximate **PLANNED** positions of **LEVELS** or the **EXISTING** levels are shown to the main spread sheet to scale. Tree heights are approximate.
- DRAINAGE - All drainage has been surveyed by visual inspection only and should be cross checked in critical areas.
- FENCES - Fences shown are not necessarily legal boundaries.
- GRID - The survey grid is based on arbitrary co-ordinates. Not Ordnance Survey.
- LEVELS - Levels relate to ODMS values.

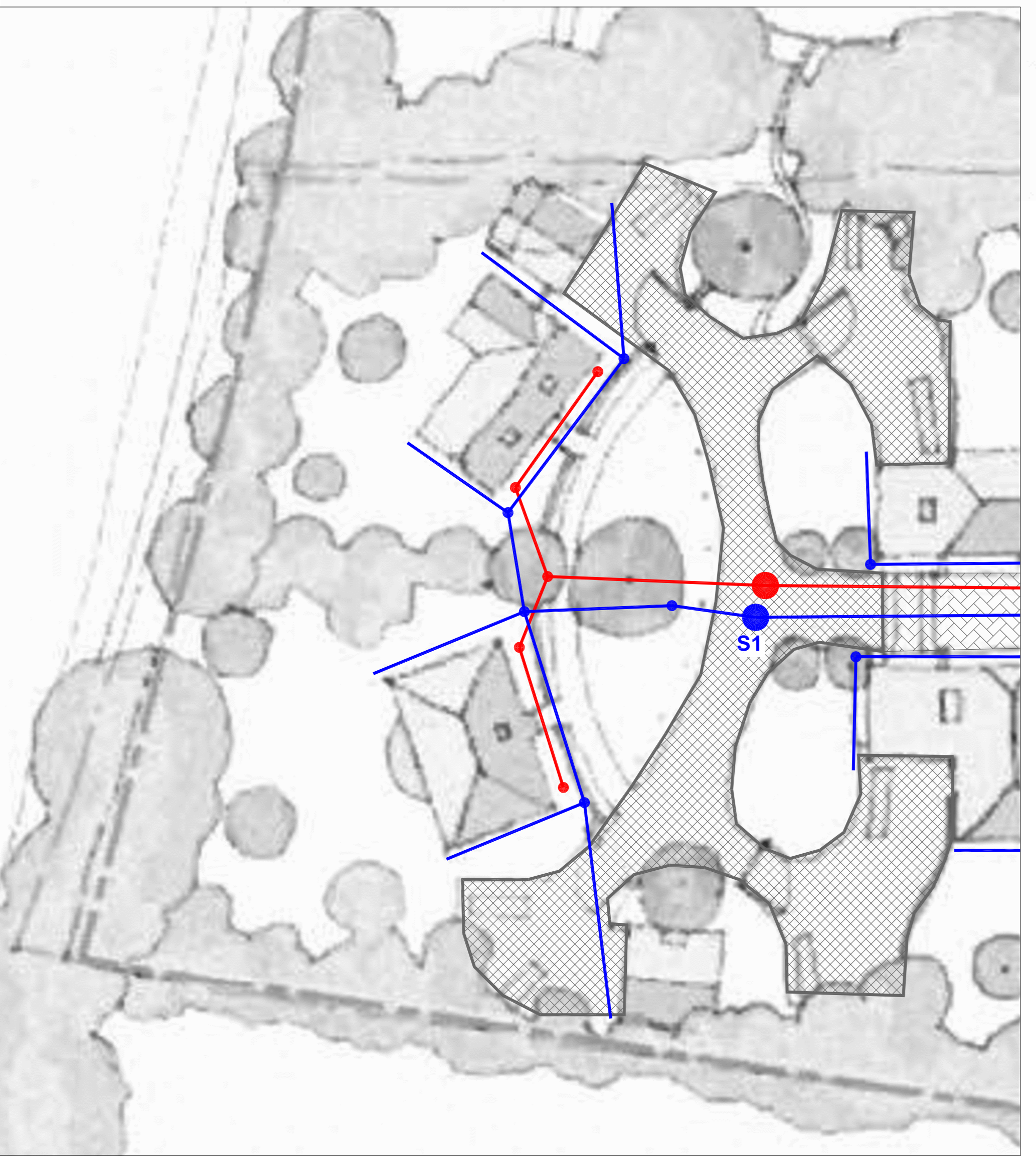


**APPENDIX C:**

Proposed Drainage Strategy Layout



- NOTES
1. ALL DIMENSIONS IN MILLIMETERS UNLESS NOTED OTHERWISE.
  2. THIS DRAWING TO BE READ IN CONJUNCTION WITH ALL OTHER ENGINEERING DRAWINGS AND CALCULATIONS ASSOCIATED WITH THIS PROJECT.
  3. POROUS PAVING DEPTH SUBJECT TO SOAKAGE TESTING IN ACCORDANCE WITH BRE365.
  4. DRAINAGE POSITIONS ARE INDICATIVE ONLY AND ARE SUBJECT TO DETAILED DESIGN.
  5. SEWERAGE TREATMENT PLANT TO BE DESIGNED AND INSTALLED IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATION AND SPECIFICATION.
  6. ALL ADAPTABLE DRAINAGE WORKS ARE TO BE CARRIED OUT TO THE REQUIREMENTS AND FULL SATISFACTION OF SOUTHERN WATER SERVICES LTD.
  7. ALL ADAPTABLE HIGHWAY WORKS ARE TO BE CARRIED OUT TO THE REQUIREMENTS AND FULL SATISFACTION OF KENT COUNTY COUNCIL.
  8. ALL SEWERS ARE TO BE CONSTRUCTED IN ACCORDANCE WITH WATER AUTHORITIES ASSOCIATION PUBLICATION 'SEWERS FOR ADOP' FOR 7TH EDITION.
  9. ALL BUILDING DRAINAGE TO BE INSTALLED AND TESTED IN COMPLIANCE WITH THE BUILDING REGULATIONS 2000 DRAINAGE AND WASTE DISPOSAL APPROVED DOCUMENT 19 2005 EDITION.
  10. ALL COMPONENTS AND MATERIALS ARE TO BE MANUFACTURED AND SUPPLIED IN ACCORDANCE WITH THE RELEVANT BRITISH STANDARDS, AND LAD AND SHIPPED IN ACCORDANCE WITH MANUFACTURERS INSTRUCTIONS AND THE RELEVANT BRITISH STANDARDS.
  11. THE CONTRACTOR SHALL, BEFORE COMMENCING THE WORKS, VERIFY ALL SITE AND SETTING OUT DIMENSIONS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE TRUE AND PROPER SETTING OUT OF THE WORKS AND FOR THE CORRECTNESS OF THE POSITION, LEVELS, DIMENSIONS AND ALIGNMENT OF ALL PARTS OF THE WORKS.
  12. SMALL LIGHTWEIGHT ACCESS COVERS SHOULD BE SECURED (FOR EXAMPLE WITH SCREWS) TO DETER UNAUTHORISED ACCESS.
  13. INSPECTION CHAMBERS AND MANHOLES IN BUILDINGS TO HAVE MECHANICALLY FIRED AIRTIGHT COVERS UNLESS THE DRAINITSELF HAS WATER TIGHT ACCESS COVERS.
  14. ALL ABOVE GROUND DRAINAGE TO INCORPORATE RODDING ACCESS FACILITIES.
  15. INSET/10 CONCRETE FOR USE IN GENERAL DRAINAGE WORKS. GRADE TO BS 5328.
  17. ALL GULLIES TO BE TRAPPED.
  18. SEWERAGE TREATMENT PLANT WILL BE SUBJECT TO ENVIRONMENTAL PERMIT APPLICATION TO THE ENVIRONMENT AGENCY.
  19. ACCESS ROAD AND DRIVES TO BE CONSTRUCTED IN POROUS PAVING MATERIAL TO COMPLY WITH WATER QUALITY REQUIREMENTS WITHIN THE SUDS MANUAL.
  20. DISCHARGE TO THE EXISTING WATERCOURSE WILL BE SUBJECT TO KENT COUNTY COUNCIL AND INTERNAL DRAINAGE BOARD APPROVAL.
  21. HIGHWAY POROUS PAVING CONSTRUCTION AND BALANCING POND TO PROVIDE SURFACE WATER ATTENUATION DURING HEAVY RAINFALL EVENTS.



**DRAWING LEGEND**

SURFACE WATER DRAINAGE	
●	PCC MANHOLE
●	INSPECTION CHAMBER
◆	450x900 ROAD GULLY
—	SURFACE WATER SEWER
▨	POROUS PAVING ROAD CONSTRUCTION
▩	POROUS PAVING DRIVE CONSTRUCTION
FOUL WATER DRAINAGE	
●	PCC MANHOLE
●	INSPECTION CHAMBER
—	FOUL WATER SEWER

PRE-DEVELOPMENT IMPERMEABLE AREA = 1.34Ha

POST DEVELOPMENT IMPERMEABLE AREA = 0.404Ha

STORM EVENT (1 IN)	EXISTING FLOW (l/s)	PROPOSED FLOW (l/s)
2	2	5.0
30	30	5.0
100	100	5.1

**360 MINUTE STORM DURATION**

STORM EVENT (1 IN)	EXISTING VOLUME (cu.m)	PROPOSED VOLUME (cu.m)
2	319.1	96.2
30	573.6	172.9
100	741.2	223.5

PROPOSED DRAINAGE CALCULATIONS INCLUDE A 30% CLIMATE CHANGE ALLOWANCE

P2	PLANNING ISSUE	13.01.16	MGC
P1	PLANNING ISSUE	29.11.14	MGC
REV	AMENDMENT	DATE	CHKD

FOR PLANNING

# RCD

RCD CONSULTANTS LTD  
 23 HASTINGS ROAD, MAIDSTONE, KENT, ME15 7QH  
 TELEPHONE: 01622 766 300 MOBILE: 07702 052 137  
 EMAIL: info@rcd-uk.com

CLIENT  
 WEALDEN HOMES

PROJECT  
 CLAYGATE ROAD  
 COLLIER STREET  
 KENT

DRAWING TITLE  
 DRAINAGE STRATEGY


## CIVILS

SCALE	DRAWN BY	CHECKED	DATE
1:200 @ A3 NTS @ A3	RAC	MGC	SEPT 2014

DRAWING NUMBER	REVISION
1129-1008-ENG-01	P2

**APPENDIX D:**

Existing Surface Water Calculations

RCD		Page 1
18 Deyley Way Singleton Ashford TN23 5HX	1129-1008-EXIST CLAYGATE ROAD COLLIER STREET	
Date JAN 2016 File 1129-1008-EXISTING 1601...	Designed by RAC Checked by	
Micro Drainage	Network 2015.1	

STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - England and Wales

Return Period (years)	2	Add Flow / Climate Change (%)	0
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.200
Ratio R	0.350	Maximum Backdrop Height (m)	1.500
Maximum Rainfall (mm/hr)	50	Min Design Depth for Optimisation (m)	1.200
Maximum Time of Concentration (mins)	30	Min Vel for Auto Design only (m/s)	1.00
Foul Sewage (l/s/ha)	0.000	Min Slope for Optimisation (1:X)	500
Volumetric Runoff Coeff.	0.750		

Designed with Level Inverts

Time Area Diagram for Storm

Time (mins)	Area (ha)	Time (mins)	Area (ha)
0-4	0.841	4-8	0.499

Total Area Contributing (ha) = 1.340

Total Pipe Volume (m³) = 45.239

Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.000	40.000	0.100	400.0	0.350	5.00	0.0	0.600	o	600
1.001	40.000	0.100	400.0	0.340	0.00	0.0	0.600	o	600
1.002	40.000	0.100	400.0	0.325	0.00	0.0	0.600	o	600
1.003	40.000	0.100	400.0	0.325	0.00	0.0	0.600	o	600

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.000	50.00	5.55	50.000	0.350	0.0	0.0	0.0	1.21	342.5	47.4
1.001	50.00	6.10	49.900	0.690	0.0	0.0	0.0	1.21	342.5	93.4
1.002	50.00	6.65	49.800	1.015	0.0	0.0	0.0	1.21	342.5	137.4
1.003	50.00	7.20	49.700	1.340	0.0	0.0	0.0	1.21	342.5	181.5




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Manhole Schedules for Storm

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam., L*W (mm)	Pipe Out		Pipes In			Backdrop (mm)
					PN	Invert Level (m)	Diameter (mm)	PN	Invert Level (m)	
1	51.000	1.000	Open Manhole	1500	1.000	50.000	600			
2	51.000	1.100	Open Manhole	1500	1.001	49.900	600	1.000	49.900	600
3	51.000	1.200	Open Manhole	1500	1.002	49.800	600	1.001	49.800	600
4	51.000	1.300	Open Manhole	1500	1.003	49.700	600	1.002	49.700	600
DITCH	51.000	1.400	Open Manhole	450		OUTFALL		1.003	49.600	600

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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	o	600	1	51.000	50.000	0.400	Open Manhole	1500
1.001	o	600	2	51.000	49.900	0.500	Open Manhole	1500
1.002	o	600	3	51.000	49.800	0.600	Open Manhole	1500
1.003	o	600	4	51.000	49.700	0.700	Open Manhole	1500

Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	40.000	400.0	2	51.000	49.900	0.500	Open Manhole	1500
1.001	40.000	400.0	3	51.000	49.800	0.600	Open Manhole	1500
1.002	40.000	400.0	4	51.000	49.700	0.700	Open Manhole	1500
1.003	40.000	400.0	DITCH	51.000	49.600	0.800	Open Manhole	450

Free Flowing Outfall Details for Storm


Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)
1.003	DITCH	51.000	49.600	49.600	450	0

Simulation Criteria for Storm

Volumetric Runoff Coeff	0.840	Foul Sewage per hectare (l/s)	0.000
Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	0.000
Hot Start (mins)	0	MADD Factor * 10m <sup>3</sup> /ha Storage	2.000
Hot Start Level (mm)	0	Run Time (mins)	60
Manhole Headloss Coeff (Global)	0.500	Output Interval (mins)	1
Number of Input Hydrographs	0	Number of Storage Structures	0
Number of Online Controls	0	Number of Time/Area Diagrams	0
Number of Offline Controls	0		

Synthetic Rainfall Details


Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	2	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Storm Duration (mins)	15
Ratio R	0.350		

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Summary of Results for 15 minute 2 year Winter (Storm)

Margin for Flood Risk Warning (mm) 300.0      DVD Status OFF  
 Analysis Timestep      Fine Inertia Status OFF  
 DTS Status      ON

PN	US/MH Name	Water			Surcharged		Flooded		Pipe	
		Level (m)	Depth (m)	Volume (m <sup>3</sup> )	Flow / Cap.	Overflow (l/s)	Flow (l/s)	Status		
1.000	1	50.232	-0.368	0.000	0.20		56.9	OK		
1.001	2	50.185	-0.315	0.000	0.34		97.9	OK		
1.002	3	50.121	-0.279	0.000	0.46		134.7	OK		
1.003	4	50.032	-0.268	0.000	0.58		169.7	OK		

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STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - England and Wales

Return Period (years)	2	Add Flow / Climate Change (%)	0
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.200
Ratio R	0.350	Maximum Backdrop Height (m)	1.500
Maximum Rainfall (mm/hr)	50	Min Design Depth for Optimisation (m)	1.200
Maximum Time of Concentration (mins)	30	Min Vel for Auto Design only (m/s)	1.00
Foul Sewage (l/s/ha)	0.000	Min Slope for Optimisation (1:X)	500
Volumetric Runoff Coeff.	0.750		

Designed with Level Inverts

Time Area Diagram for Storm

Time (mins)	Area (ha)	Time (mins)	Area (ha)
0-4	0.841	4-8	0.499

Total Area Contributing (ha) = 1.340

Total Pipe Volume (m<sup>3</sup>) = 45.239

Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.000	40.000	0.100	400.0	0.350	5.00	0.0	0.600	o	600
1.001	40.000	0.100	400.0	0.340	0.00	0.0	0.600	o	600
1.002	40.000	0.100	400.0	0.325	0.00	0.0	0.600	o	600
1.003	40.000	0.100	400.0	0.325	0.00	0.0	0.600	o	600

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.000	50.00	5.55	50.000	0.350	0.0	0.0	0.0	1.21	342.5	47.4
1.001	50.00	6.10	49.900	0.690	0.0	0.0	0.0	1.21	342.5	93.4
1.002	50.00	6.65	49.800	1.015	0.0	0.0	0.0	1.21	342.5	137.4
1.003	50.00	7.20	49.700	1.340	0.0	0.0	0.0	1.21	342.5	181.5

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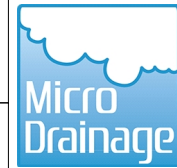


Manhole Schedules for Storm

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam., L*W (mm)	Pipe Out		Pipes In			Backdrop (mm)
					PN	Invert Level (m)	Diameter (mm)	PN	Invert Level (m)	
1	51.000	1.000	Open Manhole	1500	1.000	50.000	600			
2	51.000	1.100	Open Manhole	1500	1.001	49.900	600	1.000	49.900	600
3	51.000	1.200	Open Manhole	1500	1.002	49.800	600	1.001	49.800	600
4	51.000	1.300	Open Manhole	1500	1.003	49.700	600	1.002	49.700	600
DITCH	51.000	1.400	Open Manhole	450		OUTFALL		1.003	49.600	600

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1129-1008-EXIST  
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 COLLIER STREET



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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	o	600	1	51.000	50.000	0.400	Open Manhole	1500
1.001	o	600	2	51.000	49.900	0.500	Open Manhole	1500
1.002	o	600	3	51.000	49.800	0.600	Open Manhole	1500
1.003	o	600	4	51.000	49.700	0.700	Open Manhole	1500

Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	40.000	400.0	2	51.000	49.900	0.500	Open Manhole	1500
1.001	40.000	400.0	3	51.000	49.800	0.600	Open Manhole	1500
1.002	40.000	400.0	4	51.000	49.700	0.700	Open Manhole	1500
1.003	40.000	400.0	DITCH	51.000	49.600	0.800	Open Manhole	450

Free Flowing Outfall Details for Storm


Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)
1.003	DITCH	51.000	49.600	49.600	450	0

Simulation Criteria for Storm

Volumetric Runoff Coeff	0.840	Foul Sewage per hectare (l/s)	0.000
Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	0.000
Hot Start (mins)	0	MADD Factor * 10m <sup>3</sup> /ha Storage	2.000
Hot Start Level (mm)	0	Run Time (mins)	60
Manhole Headloss Coeff (Global)	0.500	Output Interval (mins)	1
Number of Input Hydrographs	0	Number of Storage Structures	0
Number of Online Controls	0	Number of Time/Area Diagrams	0
Number of Offline Controls	0		

Synthetic Rainfall Details


Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	30	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Storm Duration (mins)	15
Ratio R	0.350		

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Micro Drainage	Network 2015.1	

Summary of Results for 15 minute 30 year Winter (Storm)

Margin for Flood Risk Warning (mm) 300.0      DVD Status OFF  
 Analysis Timestep      Fine Inertia Status OFF  
 DTS Status      ON

PN	US/MH Name	Water		Surcharged		Flooded		Pipe Flow (l/s)	Status
		Level (m)	Depth (m)	Volume (m <sup>3</sup> )	Flow / Cap.	Overflow (l/s)			
1.000	1	50.484	-0.116	0.000	0.34		99.8	OK	
1.001	2	50.458	-0.042	0.000	0.62		181.8	OK	
1.002	3	50.400	0.000	0.000	0.88		255.7	OK	
1.003	4	50.308	0.008	0.000	1.12		327.5	SURCHARGED	

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STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - England and Wales

Return Period (years)	2	Add Flow / Climate Change (%)	0
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.200
Ratio R	0.350	Maximum Backdrop Height (m)	1.500
Maximum Rainfall (mm/hr)	50	Min Design Depth for Optimisation (m)	1.200
Maximum Time of Concentration (mins)	30	Min Vel for Auto Design only (m/s)	1.00
Foul Sewage (l/s/ha)	0.000	Min Slope for Optimisation (1:X)	500
Volumetric Runoff Coeff.	0.750		

Designed with Level Inverts

Time Area Diagram for Storm

Time (mins)	Area (ha)	Time (mins)	Area (ha)
0-4	0.841	4-8	0.499

Total Area Contributing (ha) = 1.340

Total Pipe Volume (m<sup>3</sup>) = 45.239

Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.000	40.000	0.100	400.0	0.350	5.00	0.0	0.600	o	600
1.001	40.000	0.100	400.0	0.340	0.00	0.0	0.600	o	600
1.002	40.000	0.100	400.0	0.325	0.00	0.0	0.600	o	600
1.003	40.000	0.100	400.0	0.325	0.00	0.0	0.600	o	600

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.000	50.00	5.55	50.000	0.350	0.0	0.0	0.0	1.21	342.5	47.4
1.001	50.00	6.10	49.900	0.690	0.0	0.0	0.0	1.21	342.5	93.4
1.002	50.00	6.65	49.800	1.015	0.0	0.0	0.0	1.21	342.5	137.4
1.003	50.00	7.20	49.700	1.340	0.0	0.0	0.0	1.21	342.5	181.5




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Manhole Schedules for Storm

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam., L*W (mm)	Pipe Out		Pipes In			Backdrop (mm)
					PN	Invert Level (m)	Diameter (mm)	PN	Invert Level (m)	
1	51.000	1.000	Open Manhole	1500	1.000	50.000	600			
2	51.000	1.100	Open Manhole	1500	1.001	49.900	600	1.000	49.900	600
3	51.000	1.200	Open Manhole	1500	1.002	49.800	600	1.001	49.800	600
4	51.000	1.300	Open Manhole	1500	1.003	49.700	600	1.002	49.700	600
DITCH	51.000	1.400	Open Manhole	450		OUTFALL		1.003	49.600	600

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18 Deyley Way Singleton Ashford TN23 5HX	1129-1008-EXIST CLAYGATE ROAD COLLIER STREET	
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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	o	600	1	51.000	50.000	0.400	Open Manhole	1500
1.001	o	600	2	51.000	49.900	0.500	Open Manhole	1500
1.002	o	600	3	51.000	49.800	0.600	Open Manhole	1500
1.003	o	600	4	51.000	49.700	0.700	Open Manhole	1500

Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	40.000	400.0	2	51.000	49.900	0.500	Open Manhole	1500
1.001	40.000	400.0	3	51.000	49.800	0.600	Open Manhole	1500
1.002	40.000	400.0	4	51.000	49.700	0.700	Open Manhole	1500
1.003	40.000	400.0	DITCH	51.000	49.600	0.800	Open Manhole	450

Free Flowing Outfall Details for Storm


Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)
1.003	DITCH	51.000	49.600	49.600	450	0

Simulation Criteria for Storm

Volumetric Runoff Coeff	0.840	Foul Sewage per hectare (l/s)	0.000
Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	0.000
Hot Start (mins)	0	MADD Factor * 10m <sup>3</sup> /ha Storage	2.000
Hot Start Level (mm)	0	Run Time (mins)	60
Manhole Headloss Coeff (Global)	0.500	Output Interval (mins)	1
Number of Input Hydrographs	0	Number of Storage Structures	0
Number of Online Controls	0	Number of Time/Area Diagrams	0
Number of Offline Controls	0		

Synthetic Rainfall Details

Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	100	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Storm Duration (mins)	15
Ratio R	0.350		

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18 Deyley Way Singleton Ashford TN23 5HX	1129-1008-EXIST CLAYGATE ROAD COLLIER STREET	
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Micro Drainage	Network 2015.1	

Summary of Results for 15 minute 100 year Winter (Storm)

Margin for Flood Risk Warning (mm) 300.0      DVD Status OFF  
 Analysis Timestep      Fine Inertia Status OFF  
 DTS Status      ON

PN	US/MH Name	Water			Surcharged		Flooded	Pipe		Status
		Level (m)	Depth (m)	Volume (m <sup>3</sup> )	Flow / Cap.	Overflow (l/s)	Flow (l/s)			
1.000	1	50.702	0.102	0.000	0.45		132.6		FLOOD RISK	
1.001	2	50.669	0.169	0.000	0.85		247.0		SURCHARGED	
1.002	3	50.593	0.193	0.000	1.21		352.8		SURCHARGED	
1.003	4	50.434	0.134	0.000	1.55		452.5		SURCHARGED	

18 Deyley Way  
 Singleton  
 Ashford TN23 5HX

1129-1008-EXIST  
 CLAYGATE ROAD  
 COLLIER STREET



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Source Control 2015.1

Summary of Results for 100 year Return Period

Storm Event	Max Level (m)	Max Depth (m)	Max Volume (m <sup>3</sup> )	Status
360 min Summer	50.412	4.412	661.8	O K
360 min Winter	50.942	4.942	741.2	Flood Risk

Storm Event	Rain (mm/hr)	Flooded Volume (m <sup>3</sup> )	Time-Peak (mins)
360 min Summer	10.975	0.0	368
360 min Winter	10.975	0.0	368

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 COLLIER STREET



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Rainfall Details

Rainfall Model	FSR	Winter Storms	Yes
Return Period (years)	100	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Shortest Storm (mins)	360
Ratio R	0.350	Longest Storm (mins)	360
Summer Storms	Yes	Climate Change %	+0

Time Area Diagram

Total Area (ha) 1.340

Time (mins)		Area	Time (mins)		Area
From:	To:	(ha)	From:	To:	(ha)
0	4	0.841	4	8	0.499

18 Deyley Way  
Singleton  
Ashford TN23 5HX

1129-1008-EXIST  
CLAYGATE ROAD  
COLLIER STREET



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Model Details

Storage is Online Cover Level (m) 51.000


Tank or Pond Structure

Invert Level (m) 46.000

Depth (m)	Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )
0.000	150.0	5.000	150.0

**APPENDIX E:**

Proposed Surface Water Calculations

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Micro Drainage	Network 2015.1	

STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - England and Wales			
Return Period (years)	2	Add Flow / Climate Change (%)	30
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.000
Ratio R	0.350	Maximum Backdrop Height (m)	10.000
Maximum Rainfall (mm/hr)	50	Min Design Depth for Optimisation (m)	1.200
Maximum Time of Concentration (mins)	30	Min Vel for Auto Design only (m/s)	1.00
Foul Sewage (l/s/ha)	0.000	Min Slope for Optimisation (1:X)	500
Volumetric Runoff Coeff.	0.750		

Designed with Level Inverts

Time Area Diagram for Storm

Time (mins)	Area (ha)	Time (mins)	Area (ha)	Time (mins)	Area (ha)
0-4	0.187	4-8	0.211	8-12	0.006

Total Area Contributing (ha) = 0.404

Total Pipe Volume (m<sup>3</sup>) = 66.586


Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.000	25.000	0.050	500.0	0.025	5.00	0.0	0.600	o	450
1.001	20.000	0.050	400.0	0.046	0.00	0.0	0.600	o	450
1.002	25.000	0.050	500.0	0.047	0.00	0.0	0.600	o	450
1.003	34.000	0.080	425.0	0.013	0.00	0.0	0.600	o	450
1.004	36.000	0.080	450.0	0.043	0.00	0.0	0.600	o	600
1.005	39.000	0.100	390.0	0.032	0.00	0.0	0.600	o	600
1.006	12.000	0.030	400.0	0.085	0.00	0.0	0.600	o	600

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	E I.Area (ha)	E Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.000	50.00	5.46	49.900	0.025	0.0	0.0	1.0	0.90	143.5	4.4
1.001	50.00	5.79	49.850	0.071	0.0	0.0	2.9	1.01	160.7	12.5
1.002	50.00	6.25	49.800	0.118	0.0	0.0	4.8	0.90	143.5	20.8
1.003	50.00	6.83	49.750	0.131	0.0	0.0	5.3	0.98	155.8	23.1
1.004	50.00	7.36	49.670	0.174	0.0	0.0	7.1	1.14	322.7	30.6
1.005	50.00	7.89	49.590	0.206	0.0	0.0	8.4	1.23	346.9	36.3
1.006	50.00	8.05	49.490	0.291	0.0	0.0	11.8	1.21	342.5	51.2



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Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.007	28.000	0.060	466.7	0.020	0.00	0.0	0.600	o	600
1.008	57.000	0.140	407.1	0.093	0.00	0.0	0.600	o	600
1.009	5.000	0.050	100.0	0.000	0.00	0.0	0.600	o	600

Network Results Table


PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.007	50.00	8.47	49.460	0.311	0.0	0.0	12.6	1.12	316.8	54.7
1.008	49.51	9.26	49.400	0.404	0.0	0.0	16.3	1.20	339.5	70.4
1.009	49.42	9.29	49.260	0.404	0.0	0.0	16.3	2.44	688.6	70.4

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Manhole Schedules for Storm

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam., L*W (mm)	PN	Pipe Out Invert Level (m)	Pipe Out Diameter (mm)	PN	Pipes In Invert Level (m)	Pipes In Diameter (mm)	Backdrop (mm)
1	51.000	1.100	Open Manhole	1500	1.000	49.900	450				
2	51.000	1.150	Open Manhole	1500	1.001	49.850	450	1.000	49.850	450	
3	51.000	1.200	Open Manhole	1500	1.002	49.800	450	1.001	49.800	450	
4	51.000	1.250	Open Manhole	1500	1.003	49.750	450	1.002	49.750	450	
5	51.000	1.330	Open Manhole	1500	1.004	49.670	600	1.003	49.670	450	
6	51.000	1.410	Open Manhole	1500	1.005	49.590	600	1.004	49.590	600	
7	51.000	1.510	Open Manhole	1500	1.006	49.490	600	1.005	49.490	600	
8	51.000	1.540	Open Manhole	1500	1.007	49.460	600	1.006	49.460	600	
9	51.000	1.600	Open Manhole	1500	1.008	49.400	600	1.007	49.400	600	
10	51.000	1.740	Open Manhole	1500	1.009	49.260	600	1.008	49.260	600	
	51.000	1.790	Open Manhole	450		OUTFALL		1.009	49.210	600	

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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	o	450	1	51.000	49.900	0.650	Open Manhole	1500
1.001	o	450	2	51.000	49.850	0.700	Open Manhole	1500
1.002	o	450	3	51.000	49.800	0.750	Open Manhole	1500
1.003	o	450	4	51.000	49.750	0.800	Open Manhole	1500
1.004	o	600	5	51.000	49.670	0.730	Open Manhole	1500
1.005	o	600	6	51.000	49.590	0.810	Open Manhole	1500
1.006	o	600	7	51.000	49.490	0.910	Open Manhole	1500
1.007	o	600	8	51.000	49.460	0.940	Open Manhole	1500
1.008	o	600	9	51.000	49.400	1.000	Open Manhole	1500
1.009	o	600	10	51.000	49.260	1.140	Open Manhole	1500

Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	25.000	500.0	2	51.000	49.850	0.700	Open Manhole	1500
1.001	20.000	400.0	3	51.000	49.800	0.750	Open Manhole	1500
1.002	25.000	500.0	4	51.000	49.750	0.800	Open Manhole	1500
1.003	34.000	425.0	5	51.000	49.670	0.880	Open Manhole	1500
1.004	36.000	450.0	6	51.000	49.590	0.810	Open Manhole	1500
1.005	39.000	390.0	7	51.000	49.490	0.910	Open Manhole	1500
1.006	12.000	400.0	8	51.000	49.460	0.940	Open Manhole	1500
1.007	28.000	466.7	9	51.000	49.400	1.000	Open Manhole	1500
1.008	57.000	407.1	10	51.000	49.260	1.140	Open Manhole	1500
1.009	5.000	100.0		51.000	49.210	1.190	Open Manhole	450


Free Flowing Outfall Details for Storm

Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)
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1.009		51.000	49.210	49.210	450	0
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Simulation Criteria for Storm


Volumetric Runoff Coeff	0.840	Foul Sewage per hectare (l/s)	0.000
Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	30.000
Hot Start (mins)	0	MADD Factor * 10m <sup>3</sup> /ha Storage	2.000
Hot Start Level (mm)	0	Run Time (mins)	360
Manhole Headloss Coeff (Global)	0.500	Output Interval (mins)	3
Number of Input Hydrographs	0	Number of Storage Structures	4
Number of Online Controls	2	Number of Time/Area Diagrams	0
Number of Offline Controls	0		

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Simulation Criteria for Storm

Synthetic Rainfall Details

Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	2	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Storm Duration (mins)	180
Ratio R	0.350		

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Online Controls for Storm

Hydro-Brake Optimum® Manhole: 7, DS/PN: 1.006, Volume (m³): 13.3

Unit Reference MD-SHE-0105-5000-1000-5000  
 Design Head (m) 1.000  
 Design Flow (l/s) 5.0  
 Flush-Flo™ Calculated  
 Objective Minimise upstream storage  
 Diameter (mm) 105  
 Invert Level (m) 49.490  
 Minimum Outlet Pipe Diameter (mm) 150  
 Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.000	5.0
Flush-Flo™	0.295	4.9
Kick-Flo®	0.636	4.0
Mean Flow over Head Range	-	4.3


The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	3.6	1.200	5.4	3.000	8.3	7.000	12.4
0.200	4.8	1.400	5.8	3.500	8.9	7.500	12.8
0.300	4.9	1.600	6.2	4.000	9.5	8.000	13.2
0.400	4.9	1.800	6.5	4.500	10.1	8.500	13.6
0.500	4.7	2.000	6.9	5.000	10.6	9.000	14.0
0.600	4.3	2.200	7.2	5.500	11.1	9.500	14.4
0.800	4.5	2.400	7.5	6.000	11.5		
1.000	5.0	2.600	7.8	6.500	12.0		

Hydro-Brake Optimum® Manhole: 10, DS/PN: 1.009, Volume (m³): 18.8

Unit Reference MD-SHE-0100-5000-1350-5000  
 Design Head (m) 1.350  
 Design Flow (l/s) 5.0  
 Flush-Flo™ Calculated  
 Objective Minimise upstream storage  
 Diameter (mm) 100  
 Invert Level (m) 49.260  
 Minimum Outlet Pipe Diameter (mm) 150  
 Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.350	5.0
Flush-Flo™	0.401	5.0


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Hydro-Brake Optimum® Manhole: 10, DS/PN: 1.009, Volume (m³): 18.8

Control Points	Head (m)	Flow (l/s)
Kick-Flo®	0.825	4.0
Mean Flow over Head Range	-	4.4

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	3.3	1.200	4.7	3.000	7.3	7.000	10.8
0.200	4.6	1.400	5.1	3.500	7.8	7.500	11.2
0.300	4.9	1.600	5.4	4.000	8.3	8.000	11.6
0.400	5.0	1.800	5.7	4.500	8.8	8.500	11.9
0.500	4.9	2.000	6.0	5.000	9.2	9.000	12.2
0.600	4.8	2.200	6.3	5.500	9.7	9.500	12.5
0.800	4.1	2.400	6.5	6.000	10.1		
1.000	4.3	2.600	6.8	6.500	10.5		

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Storage Structures for Storm

Porous Car Park Manhole: 3, DS/PN: 1.002

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	10.0
Membrane Percolation (mm/hr)	1000	Length (m)	34.0
Max Percolation (l/s)	94.4	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000

Tank or Pond Manhole: 5, DS/PN: 1.004

Invert Level (m) 50.000


Depth (m)	Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )
0.000	40.0	1.000	100.0

Porous Car Park Manhole: 7, DS/PN: 1.006

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.0
Membrane Percolation (mm/hr)	1000	Length (m)	120.0
Max Percolation (l/s)	166.7	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000

Porous Car Park Manhole: 10, DS/PN: 1.009

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.0
Membrane Percolation (mm/hr)	1000	Length (m)	92.0
Max Percolation (l/s)	127.8	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000


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Summary of Results for 180 minute 2 year Winter (Storm)

Margin for Flood Risk Warning (mm) 300.0      DVD Status OFF  
 Analysis Timestep      Fine Inertia Status OFF  
 DTS Status      ON

PN	US/MH Name	Water			Surcharged		Flooded		Pipe	
		Level (m)	Depth (m)	Volume (m <sup>3</sup> )	Flow / Cap.	Overflow (l/s)	Flow (l/s)	Status		
1.000	1	50.058	-0.292	0.000	0.01		1.4	OK		
1.001	2	50.058	-0.242	0.000	0.03		3.8	OK		
1.002	3	50.057	-0.193	0.000	0.05		6.1	OK		
1.003	4	50.057	-0.143	0.000	0.04		6.0	OK		
1.004	5	50.056	-0.214	0.000	0.02		6.5	OK		
1.005	6	50.056	-0.134	0.000	0.02		5.1	OK		
1.006	7	50.055	-0.035	0.000	0.03		4.9	OK		
1.007	8	49.856	-0.204	0.000	0.02		5.6	OK		
1.008	9	49.855	-0.145	0.000	0.03		9.0	OK		
1.009	10	49.854	-0.006	0.000	0.01		5.0	OK		



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STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - England and Wales			
Return Period (years)	2	Add Flow / Climate Change (%)	30
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.000
Ratio R	0.350	Maximum Backdrop Height (m)	10.000
Maximum Rainfall (mm/hr)	50	Min Design Depth for Optimisation (m)	1.200
Maximum Time of Concentration (mins)	30	Min Vel for Auto Design only (m/s)	1.00
Foul Sewage (l/s/ha)	0.000	Min Slope for Optimisation (1:X)	500
Volumetric Runoff Coeff.	0.750		

Designed with Level Inverts

Time Area Diagram for Storm

Time (mins)	Area (ha)	Time (mins)	Area (ha)	Time (mins)	Area (ha)
0-4	0.187	4-8	0.211	8-12	0.006

Total Area Contributing (ha) = 0.404


Total Pipe Volume (m<sup>3</sup>) = 66.586

Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.000	25.000	0.050	500.0	0.025	5.00	0.0	0.600	o	450
1.001	20.000	0.050	400.0	0.046	0.00	0.0	0.600	o	450
1.002	25.000	0.050	500.0	0.047	0.00	0.0	0.600	o	450
1.003	34.000	0.080	425.0	0.013	0.00	0.0	0.600	o	450
1.004	36.000	0.080	450.0	0.043	0.00	0.0	0.600	o	600
1.005	39.000	0.100	390.0	0.032	0.00	0.0	0.600	o	600
1.006	12.000	0.030	400.0	0.085	0.00	0.0	0.600	o	600

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	E I.Area (ha)	E Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.000	50.00	5.46	49.900	0.025	0.0	0.0	1.0	0.90	143.5	4.4
1.001	50.00	5.79	49.850	0.071	0.0	0.0	2.9	1.01	160.7	12.5
1.002	50.00	6.25	49.800	0.118	0.0	0.0	4.8	0.90	143.5	20.8
1.003	50.00	6.83	49.750	0.131	0.0	0.0	5.3	0.98	155.8	23.1
1.004	50.00	7.36	49.670	0.174	0.0	0.0	7.1	1.14	322.7	30.6
1.005	50.00	7.89	49.590	0.206	0.0	0.0	8.4	1.23	346.9	36.3
1.006	50.00	8.05	49.490	0.291	0.0	0.0	11.8	1.21	342.5	51.2

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Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.007	28.000	0.060	466.7	0.020	0.00	0.0	0.600	o	600
1.008	57.000	0.140	407.1	0.093	0.00	0.0	0.600	o	600
1.009	5.000	0.050	100.0	0.000	0.00	0.0	0.600	o	600

Network Results Table


PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.007	50.00	8.47	49.460	0.311	0.0	0.0	12.6	1.12	316.8	54.7
1.008	49.51	9.26	49.400	0.404	0.0	0.0	16.3	1.20	339.5	70.4
1.009	49.42	9.29	49.260	0.404	0.0	0.0	16.3	2.44	688.6	70.4

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Manhole Schedules for Storm

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam., L*W (mm)	PN	Pipe Out Invert Level (m)	Pipe Out Diameter (mm)	PN	Pipes In Invert Level (m)	Pipes In Diameter (mm)	Backdrop (mm)
1	51.000	1.100	Open Manhole	1500	1.000	49.900	450				
2	51.000	1.150	Open Manhole	1500	1.001	49.850	450	1.000	49.850	450	
3	51.000	1.200	Open Manhole	1500	1.002	49.800	450	1.001	49.800	450	
4	51.000	1.250	Open Manhole	1500	1.003	49.750	450	1.002	49.750	450	
5	51.000	1.330	Open Manhole	1500	1.004	49.670	600	1.003	49.670	450	
6	51.000	1.410	Open Manhole	1500	1.005	49.590	600	1.004	49.590	600	
7	51.000	1.510	Open Manhole	1500	1.006	49.490	600	1.005	49.490	600	
8	51.000	1.540	Open Manhole	1500	1.007	49.460	600	1.006	49.460	600	
9	51.000	1.600	Open Manhole	1500	1.008	49.400	600	1.007	49.400	600	
10	51.000	1.740	Open Manhole	1500	1.009	49.260	600	1.008	49.260	600	
	51.000	1.790	Open Manhole	450		OUTFALL		1.009	49.210	600	

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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	o	450	1	51.000	49.900	0.650	Open Manhole	1500
1.001	o	450	2	51.000	49.850	0.700	Open Manhole	1500
1.002	o	450	3	51.000	49.800	0.750	Open Manhole	1500
1.003	o	450	4	51.000	49.750	0.800	Open Manhole	1500
1.004	o	600	5	51.000	49.670	0.730	Open Manhole	1500
1.005	o	600	6	51.000	49.590	0.810	Open Manhole	1500
1.006	o	600	7	51.000	49.490	0.910	Open Manhole	1500
1.007	o	600	8	51.000	49.460	0.940	Open Manhole	1500
1.008	o	600	9	51.000	49.400	1.000	Open Manhole	1500
1.009	o	600	10	51.000	49.260	1.140	Open Manhole	1500

Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	25.000	500.0	2	51.000	49.850	0.700	Open Manhole	1500
1.001	20.000	400.0	3	51.000	49.800	0.750	Open Manhole	1500
1.002	25.000	500.0	4	51.000	49.750	0.800	Open Manhole	1500
1.003	34.000	425.0	5	51.000	49.670	0.880	Open Manhole	1500
1.004	36.000	450.0	6	51.000	49.590	0.810	Open Manhole	1500
1.005	39.000	390.0	7	51.000	49.490	0.910	Open Manhole	1500
1.006	12.000	400.0	8	51.000	49.460	0.940	Open Manhole	1500
1.007	28.000	466.7	9	51.000	49.400	1.000	Open Manhole	1500
1.008	57.000	407.1	10	51.000	49.260	1.140	Open Manhole	1500
1.009	5.000	100.0		51.000	49.210	1.190	Open Manhole	450


Free Flowing Outfall Details for Storm

Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)
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1.009		51.000	49.210	49.210	450	0
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Simulation Criteria for Storm


Volumetric Runoff Coeff	0.840	Foul Sewage per hectare (l/s)	0.000
Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	30.000
Hot Start (mins)	0	MADD Factor * 10m <sup>3</sup> /ha Storage	2.000
Hot Start Level (mm)	0	Run Time (mins)	360
Manhole Headloss Coeff (Global)	0.500	Output Interval (mins)	3
Number of Input Hydrographs	0	Number of Storage Structures	4
Number of Online Controls	2	Number of Time/Area Diagrams	0
Number of Offline Controls	0		

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Simulation Criteria for Storm

Synthetic Rainfall Details

Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	30	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Storm Duration (mins)	180
Ratio R	0.350		

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Online Controls for Storm

Hydro-Brake Optimum® Manhole: 7, DS/PN: 1.006, Volume (m³): 13.3

Unit Reference MD-SHE-0105-5000-1000-5000  
 Design Head (m) 1.000  
 Design Flow (l/s) 5.0  
 Flush-Flo™ Calculated  
 Objective Minimise upstream storage  
 Diameter (mm) 105  
 Invert Level (m) 49.490  
 Minimum Outlet Pipe Diameter (mm) 150  
 Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.000	5.0
Flush-Flo™	0.295	4.9
Kick-Flo®	0.636	4.0
Mean Flow over Head Range	-	4.3


The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	3.6	1.200	5.4	3.000	8.3	7.000	12.4
0.200	4.8	1.400	5.8	3.500	8.9	7.500	12.8
0.300	4.9	1.600	6.2	4.000	9.5	8.000	13.2
0.400	4.9	1.800	6.5	4.500	10.1	8.500	13.6
0.500	4.7	2.000	6.9	5.000	10.6	9.000	14.0
0.600	4.3	2.200	7.2	5.500	11.1	9.500	14.4
0.800	4.5	2.400	7.5	6.000	11.5		
1.000	5.0	2.600	7.8	6.500	12.0		

Hydro-Brake Optimum® Manhole: 10, DS/PN: 1.009, Volume (m³): 18.8

Unit Reference MD-SHE-0100-5000-1350-5000  
 Design Head (m) 1.350  
 Design Flow (l/s) 5.0  
 Flush-Flo™ Calculated  
 Objective Minimise upstream storage  
 Diameter (mm) 100  
 Invert Level (m) 49.260  
 Minimum Outlet Pipe Diameter (mm) 150  
 Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.350	5.0
Flush-Flo™	0.401	5.0


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Hydro-Brake Optimum® Manhole: 10, DS/PN: 1.009, Volume (m³): 18.8

Control Points	Head (m)	Flow (l/s)
Kick-Flo®	0.825	4.0
Mean Flow over Head Range	-	4.4

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	3.3	1.200	4.7	3.000	7.3	7.000	10.8
0.200	4.6	1.400	5.1	3.500	7.8	7.500	11.2
0.300	4.9	1.600	5.4	4.000	8.3	8.000	11.6
0.400	5.0	1.800	5.7	4.500	8.8	8.500	11.9
0.500	4.9	2.000	6.0	5.000	9.2	9.000	12.2
0.600	4.8	2.200	6.3	5.500	9.7	9.500	12.5
0.800	4.1	2.400	6.5	6.000	10.1		
1.000	4.3	2.600	6.8	6.500	10.5		

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Storage Structures for Storm

Porous Car Park Manhole: 3, DS/PN: 1.002

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	10.0
Membrane Percolation (mm/hr)	1000	Length (m)	34.0
Max Percolation (l/s)	94.4	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000

Tank or Pond Manhole: 5, DS/PN: 1.004

Invert Level (m) 50.000

Depth (m)	Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )
0.000	40.0	1.000	100.0


Porous Car Park Manhole: 7, DS/PN: 1.006

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.0
Membrane Percolation (mm/hr)	1000	Length (m)	120.0
Max Percolation (l/s)	166.7	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000

Porous Car Park Manhole: 10, DS/PN: 1.009

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.0
Membrane Percolation (mm/hr)	1000	Length (m)	92.0
Max Percolation (l/s)	127.8	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000




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Summary of Results for 180 minute 30 year Winter (Storm)

Margin for Flood Risk Warning (mm) 300.0      DVD Status OFF  
 Analysis Timestep      Fine Inertia Status OFF  
 DTS Status      ON

PN	US/MH Name	Water			Flow / Cap.	Overflow (1/s)	Pipe Flow (1/s)	Status
		Level (m)	Depth (m)	Volume (m <sup>3</sup> )				
1.000	1	50.598	0.248	0.000	0.02	2.4	SURCHARGED	
1.001	2	50.599	0.299	0.000	0.05	6.5	SURCHARGED	
1.002	3	50.599	0.349	0.000	0.08	9.5	SURCHARGED	
1.003	4	50.598	0.398	0.000	0.06	8.7	SURCHARGED	
1.004	5	50.597	0.327	0.000	0.14	38.1	SURCHARGED	
1.005	6	50.597	0.407	0.000	0.07	19.4	SURCHARGED	
1.006	7	50.597	0.507	0.000	0.03	4.9	SURCHARGED	
1.007	8	50.540	0.480	0.000	0.02	5.6	SURCHARGED	
1.008	9	50.540	0.540	0.000	0.04	11.2	SURCHARGED	
1.009	10	50.538	0.678	0.000	0.01	5.0	SURCHARGED	

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STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - England and Wales			
Return Period (years)	2	Add Flow / Climate Change (%)	30
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.000
Ratio R	0.350	Maximum Backdrop Height (m)	10.000
Maximum Rainfall (mm/hr)	50	Min Design Depth for Optimisation (m)	1.200
Maximum Time of Concentration (mins)	30	Min Vel for Auto Design only (m/s)	1.00
Foul Sewage (l/s/ha)	0.000	Min Slope for Optimisation (1:X)	500
Volumetric Runoff Coeff.	0.750		

Designed with Level Inverts

Time Area Diagram for Storm

Time (mins)	Area (ha)	Time (mins)	Area (ha)	Time (mins)	Area (ha)
0-4	0.187	4-8	0.211	8-12	0.006

Total Area Contributing (ha) = 0.404


Total Pipe Volume (m<sup>3</sup>) = 66.586

Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.000	25.000	0.050	500.0	0.025	5.00	0.0	0.600	o	450
1.001	20.000	0.050	400.0	0.046	0.00	0.0	0.600	o	450
1.002	25.000	0.050	500.0	0.047	0.00	0.0	0.600	o	450
1.003	34.000	0.080	425.0	0.013	0.00	0.0	0.600	o	450
1.004	36.000	0.080	450.0	0.043	0.00	0.0	0.600	o	600
1.005	39.000	0.100	390.0	0.032	0.00	0.0	0.600	o	600
1.006	12.000	0.030	400.0	0.085	0.00	0.0	0.600	o	600

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	E I.Area (ha)	E Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.000	50.00	5.46	49.900	0.025	0.0	0.0	1.0	0.90	143.5	4.4
1.001	50.00	5.79	49.850	0.071	0.0	0.0	2.9	1.01	160.7	12.5
1.002	50.00	6.25	49.800	0.118	0.0	0.0	4.8	0.90	143.5	20.8
1.003	50.00	6.83	49.750	0.131	0.0	0.0	5.3	0.98	155.8	23.1
1.004	50.00	7.36	49.670	0.174	0.0	0.0	7.1	1.14	322.7	30.6
1.005	50.00	7.89	49.590	0.206	0.0	0.0	8.4	1.23	346.9	36.3
1.006	50.00	8.05	49.490	0.291	0.0	0.0	11.8	1.21	342.5	51.2

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Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	HYD SECT	DIA (mm)
1.007	28.000	0.060	466.7	0.020	0.00	0.0	0.600	o	600
1.008	57.000	0.140	407.1	0.093	0.00	0.0	0.600	o	600
1.009	5.000	0.050	100.0	0.000	0.00	0.0	0.600	o	600

Network Results Table


PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
1.007	50.00	8.47	49.460	0.311	0.0	0.0	12.6	1.12	316.8	54.7
1.008	49.51	9.26	49.400	0.404	0.0	0.0	16.3	1.20	339.5	70.4
1.009	49.42	9.29	49.260	0.404	0.0	0.0	16.3	2.44	688.6	70.4

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Manhole Schedules for Storm

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam., L*W (mm)	PN	Pipe Out Invert Level (m)	Pipe Out Diameter (mm)	PN	Pipes In Invert Level (m)	Pipes In Diameter (mm)	Backdrop (mm)
1	51.000	1.100	Open Manhole	1500	1.000	49.900	450				
2	51.000	1.150	Open Manhole	1500	1.001	49.850	450	1.000	49.850	450	
3	51.000	1.200	Open Manhole	1500	1.002	49.800	450	1.001	49.800	450	
4	51.000	1.250	Open Manhole	1500	1.003	49.750	450	1.002	49.750	450	
5	51.000	1.330	Open Manhole	1500	1.004	49.670	600	1.003	49.670	450	
6	51.000	1.410	Open Manhole	1500	1.005	49.590	600	1.004	49.590	600	
7	51.000	1.510	Open Manhole	1500	1.006	49.490	600	1.005	49.490	600	
8	51.000	1.540	Open Manhole	1500	1.007	49.460	600	1.006	49.460	600	
9	51.000	1.600	Open Manhole	1500	1.008	49.400	600	1.007	49.400	600	
10	51.000	1.740	Open Manhole	1500	1.009	49.260	600	1.008	49.260	600	
	51.000	1.790	Open Manhole	450		OUTFALL		1.009	49.210	600	

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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	o	450	1	51.000	49.900	0.650	Open Manhole	1500
1.001	o	450	2	51.000	49.850	0.700	Open Manhole	1500
1.002	o	450	3	51.000	49.800	0.750	Open Manhole	1500
1.003	o	450	4	51.000	49.750	0.800	Open Manhole	1500
1.004	o	600	5	51.000	49.670	0.730	Open Manhole	1500
1.005	o	600	6	51.000	49.590	0.810	Open Manhole	1500
1.006	o	600	7	51.000	49.490	0.910	Open Manhole	1500
1.007	o	600	8	51.000	49.460	0.940	Open Manhole	1500
1.008	o	600	9	51.000	49.400	1.000	Open Manhole	1500
1.009	o	600	10	51.000	49.260	1.140	Open Manhole	1500

Downstream Manhole

PN	Length (m)	Slope (1:X)	MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	25.000	500.0	2	51.000	49.850	0.700	Open Manhole	1500
1.001	20.000	400.0	3	51.000	49.800	0.750	Open Manhole	1500
1.002	25.000	500.0	4	51.000	49.750	0.800	Open Manhole	1500
1.003	34.000	425.0	5	51.000	49.670	0.880	Open Manhole	1500
1.004	36.000	450.0	6	51.000	49.590	0.810	Open Manhole	1500
1.005	39.000	390.0	7	51.000	49.490	0.910	Open Manhole	1500
1.006	12.000	400.0	8	51.000	49.460	0.940	Open Manhole	1500
1.007	28.000	466.7	9	51.000	49.400	1.000	Open Manhole	1500
1.008	57.000	407.1	10	51.000	49.260	1.140	Open Manhole	1500
1.009	5.000	100.0		51.000	49.210	1.190	Open Manhole	450


Free Flowing Outfall Details for Storm

Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)
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1.009		51.000	49.210	49.210	450	0
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Simulation Criteria for Storm


Volumetric Runoff Coeff	0.840	Foul Sewage per hectare (l/s)	0.000
Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	30.000
Hot Start (mins)	0	MADD Factor * 10m <sup>3</sup> /ha Storage	2.000
Hot Start Level (mm)	0	Run Time (mins)	360
Manhole Headloss Coeff (Global)	0.500	Output Interval (mins)	3
Number of Input Hydrographs	0	Number of Storage Structures	4
Number of Online Controls	2	Number of Time/Area Diagrams	0
Number of Offline Controls	0		

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Simulation Criteria for Storm

Synthetic Rainfall Details

Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	100	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Storm Duration (mins)	180
Ratio R	0.350		

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Online Controls for Storm

Hydro-Brake Optimum® Manhole: 7, DS/PN: 1.006, Volume (m³): 13.3

Unit Reference MD-SHE-0105-5000-1000-5000  
 Design Head (m) 1.000  
 Design Flow (l/s) 5.0  
 Flush-Flo™ Calculated  
 Objective Minimise upstream storage  
 Diameter (mm) 105  
 Invert Level (m) 49.490  
 Minimum Outlet Pipe Diameter (mm) 150  
 Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.000	5.0
Flush-Flo™	0.295	4.9
Kick-Flo®	0.636	4.0
Mean Flow over Head Range	-	4.3


The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	3.6	1.200	5.4	3.000	8.3	7.000	12.4
0.200	4.8	1.400	5.8	3.500	8.9	7.500	12.8
0.300	4.9	1.600	6.2	4.000	9.5	8.000	13.2
0.400	4.9	1.800	6.5	4.500	10.1	8.500	13.6
0.500	4.7	2.000	6.9	5.000	10.6	9.000	14.0
0.600	4.3	2.200	7.2	5.500	11.1	9.500	14.4
0.800	4.5	2.400	7.5	6.000	11.5		
1.000	5.0	2.600	7.8	6.500	12.0		

Hydro-Brake Optimum® Manhole: 10, DS/PN: 1.009, Volume (m³): 18.8

Unit Reference MD-SHE-0100-5000-1350-5000  
 Design Head (m) 1.350  
 Design Flow (l/s) 5.0  
 Flush-Flo™ Calculated  
 Objective Minimise upstream storage  
 Diameter (mm) 100  
 Invert Level (m) 49.260  
 Minimum Outlet Pipe Diameter (mm) 150  
 Suggested Manhole Diameter (mm) 1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.350	5.0
Flush-Flo™	0.401	5.0

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Hydro-Brake Optimum® Manhole: 10, DS/PN: 1.009, Volume (m³): 18.8

Control Points	Head (m)	Flow (l/s)
Kick-Flo®	0.825	4.0
Mean Flow over Head Range	-	4.4

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake Optimum® as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	3.3	1.200	4.7	3.000	7.3	7.000	10.8
0.200	4.6	1.400	5.1	3.500	7.8	7.500	11.2
0.300	4.9	1.600	5.4	4.000	8.3	8.000	11.6
0.400	5.0	1.800	5.7	4.500	8.8	8.500	11.9
0.500	4.9	2.000	6.0	5.000	9.2	9.000	12.2
0.600	4.8	2.200	6.3	5.500	9.7	9.500	12.5
0.800	4.1	2.400	6.5	6.000	10.1		
1.000	4.3	2.600	6.8	6.500	10.5		



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Micro Drainage	Network 2015.1	

Storage Structures for Storm

Porous Car Park Manhole: 3, DS/PN: 1.002

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	10.0
Membrane Percolation (mm/hr)	1000	Length (m)	34.0
Max Percolation (l/s)	94.4	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000

Tank or Pond Manhole: 5, DS/PN: 1.004

Invert Level (m) 50.000


Depth (m)	Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )
0.000	40.0	1.000	100.0

Porous Car Park Manhole: 7, DS/PN: 1.006

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.0
Membrane Percolation (mm/hr)	1000	Length (m)	120.0
Max Percolation (l/s)	166.7	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000

Porous Car Park Manhole: 10, DS/PN: 1.009


Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.0
Membrane Percolation (mm/hr)	1000	Length (m)	92.0
Max Percolation (l/s)	127.8	Slope (1:X)	1000.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	50.500	Cap Volume Depth (m)	0.000

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Summary of Results for 180 minute 100 year Winter (Storm)

Margin for Flood Risk Warning (mm) 300.0      DVD Status OFF  
 Analysis Timestep    Fine Inertia Status OFF  
 DTS Status            ON


PN	US/MH Name	Water			Surcharged		Flooded		Pipe Flow (1/s)	Status
		Level (m)	Depth (m)	Volume (m <sup>3</sup> )	Flow / Cap.	Overflow (1/s)				
1.000	1	50.719	0.369	0.000	0.03			3.0	FLOOD RISK	
1.001	2	50.719	0.419	0.000	0.06			8.4	FLOOD RISK	
1.002	3	50.719	0.469	0.000	0.10			12.3	FLOOD RISK	
1.003	4	50.719	0.519	0.000	0.10			13.3	FLOOD RISK	
1.004	5	50.718	0.448	0.000	0.02			6.4	FLOOD RISK	
1.005	6	50.718	0.528	0.000	0.02			5.3	FLOOD RISK	
1.006	7	50.718	0.628	0.000	0.03			4.9	FLOOD RISK	
1.007	8	50.634	0.574	0.000	0.02			5.5	SURCHARGED	
1.008	9	50.635	0.635	0.000	0.04			13.5	SURCHARGED	
1.009	10	50.633	0.773	0.000	0.01			5.1	SURCHARGED	

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Summary of Results for 100 year Return Period

<b>Storm Event</b>	<b>Max Level (m)</b>	<b>Max Depth (m)</b>	<b>Max Volume (m<sup>3</sup>)</b>	<b>Status</b>
360 min Summer	47.330	1.330	199.5	O K
360 min Winter	47.490	1.490	223.5	O K

<b>Storm Event</b>	<b>Rain (mm/hr)</b>	<b>Flooded Volume (m<sup>3</sup>)</b>	<b>Time-Peak (mins)</b>
360 min Summer	10.975	0.0	372
360 min Winter	10.975	0.0	372

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Rainfall Details

Rainfall Model	FSR	Winter Storms	Yes
Return Period (years)	100	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	20.000	Shortest Storm (mins)	360
Ratio R	0.350	Longest Storm (mins)	360
Summer Storms	Yes	Climate Change %	+0

Time Area Diagram

Total Area (ha) 0.404

Time (mins)	Area	Time (mins)	Area	Time (mins)	Area
From:	To:	(ha)	From:	To:	(ha)
0	4	0.187	4	8	0.211
			8	12	0.006

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Model Details

Storage is Online Cover Level (m) 51.000

Tank or Pond Structure

Invert Level (m) 46.000

Depth (m)	Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )
0.000	150.0	5.000	150.0

**APPENDIX F:**

**Conditions and Limitations**

1. This report is for planning purposes and does not constitute a design document. It is the duty of the project designers, to confirm the content of this report and to design the scheme in accordance with their own research and other extraneous parameters.
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