





# Flood Risk Assessment

Land off Plover Road, Minster, Sheppey

## Client

Dalemarch (Sheppey) Ltd No 1 Lonsdale Gardens Tunbridge Wells Kent TN1 1NU Ref: 7267 Date: May 2018

## **Consulting Engineers**

GTA Civils Ltd Gloucester House 66a Church Walk Burgess Hill West Sussex RH15 9AS

Tel: 01444 871444

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Issue	Issue date	Compiled	Checked
Preliminary Issue	02 May 2018	JP	MR
First Issue	04 June 2018	JP	MR
Second Issue	20 September 2018	JP	MR

Report by: John Pakenham BSc (Hons) Checked by: Martin Roberts I Eng, ACIWEM, MCIHT





## **Executive Summary**

- The proposal is for a development of 30 new dwellings on agricultural land to the south side of the Parsonage.
- The site is in Flood Zone 1 as indicated by the Environment Agency Flood Map, i.e. in an area having a low annual probability of flooding from fluvial sources.
- Other flood sources have been assessed surface water/overland flow, sewers, groundwater, overland flow and artificial. This site is at 'Low Risk' of flooding.
- The proposed dwelling units will be set 0.15m above ambient ground levels: no flood mitigation measures are proposed.
- SUDS: to comply with NPPF, surface water drainage systems must be designed with sustainability in mind. Due to the Clay geology, the ideal choice of infiltration is not feasible here: the soil will not possess sufficiently high permeability for soaking away.
- The surface water drainage strategy utilises a combination of porous pavings and tank. There will be 2 control manholes above the terminal offsite control. These will restrict flows *within* the site to a lower rate than is usual.
- The offsite (terminal) rate into the ditch at the NW corner will be restricted to the practical minimum limit of vortex devices, namely 2.0l/s in the critical storm. The greenfield Qbar runoff rate is 1.1 litre/second.
- The tank and porous pavings have been sized to store the storm water volume in the critical '1 in 100 years plus 40% climate change' event. The proposed drainage layout is shown in Appendix D.
- The filtering quality of pavings' sub-bases will provide treatment (cleanse the water); no other pollution control is necessary for residential dwellings.
- The foul drainage will be routed into the public foul sewerage network under gravity, following a Section 106 application and permission from Southern Water.



## 1 Introduction

- 1.1 This report has been prepared for Dalemarch (Sheppey) Ltd in relation to Land off Plover Road, Minster, Sheppey, ME12 3BT. No responsibility is accepted to any third party for all or part of this study in connection with this or any other development.
- 1.2 GTA Civils Ltd. was appointed by the client to provide a Flood Risk Assessment (FRA) as required by the Environment Agency and Swale Borough Council in order to achieve Planning Approval at said property.
- 1.3 This report will take the form of a formal Flood Risk Assessment in accordance with the 2018 National Planning Policy Framework (NPPF) and the 2015 Planning Practice Guidance (PPG).
- 1.4 The second version of this report has been prepared following an objection notice from the Lower Medway Internal Drainage Board. Sections 2.6 and 3.3 – plus the topographic survey and drainage strategy layout have been amended/corrected.



# 2 Existing Site and Current Flood Conditions

- 2.1 The application site lies within the area administered by Swale Borough Council (SBC). A site location map and aerial view are shown in Appendix A.
- 2.2 The site is currently a vacant, greenfield site. Along the eastern boundary is an un-named ditch, on the other side of which is a residential site. To the northeast of the site is agricultural land.
- 2.3 The area of the existing site is approximately 7700m<sup>2</sup> (0.77ha) and is accessed from Yarrow Drive (off Plover Road) to the northwest.
- 2.4 The site slopes from southwest to northeast. The levels range from 16.7m AOD at the south corner to 13.1m AOD at the north corner. The existing site levels are indicated on the topographic survey in Appendix B.
- 2.5 The site is underlain with London Clay according to the BGS online geological map, with no recorded drift deposits overlying it. The soil type is likely to have low permeability.
- 2.6 Hydrology: an unnamed drain/brook flows northwest, approximately 250m northeast of the east corner at its closest. This discharges into the Barton Point and Queenborough Lines, which flows into the Thames Estuary. There is a ditch that flows southeast through the site. This serves the residential development in Clover Court to the west and so has flowing water in it. This is shown on the topographic survey in Appendix B. (It shall be diverted to outside the site's NE boundary as set out on the drainage strategy layout in Appendix D. This diversion shall be subject to the IDB's permission).
- 2.7 Public sewers: Southern Water's sewer records for this area (see Appendix B) show a 150mm diameter foul main sewer (ref 4101) in Plover Road to the southwest. Nearby there is a storm water head of run (ref 4150), which is 525mm diameter. Both of these are at a higher elevation to this site, however. It is understood that there is a foul manhole available to the NW adjacent to the play area to the east of the existing houses off Yarrow Drive/clover Close.
- 2.8 The site is free draining to the ditch along the northeast and to the land to the north, which subsequently drains to a stream along its northern boundary.
- 2.9 The adjacent existing social housing site to the northwest, is currently draining to the ditch which runs across the proposed food store site. The surface water run-off from this



site is restricted to 4.0l/s for the roofs and parking courts, and a further 4.0l/s restricted outfall for the highway drainage.

2.10 A greenfield run-off calculation has been carried out in Micro Drainage using the ICP SUDS method which is contained in Appendix E. This shows an existing Q<sub>bar</sub> greenfield run-off from the aggregated contributing area (ie to be positively drained, 3214m<sup>2</sup>) of 4.71/s. The greenfield runoff rates for the post-development contributing area are as follows:

- 2.11 Fluvial Flood risk: The Environment Agency's Flood Map for Planning (Rivers and Seas) in Appendix C shows that the site is within Flood Zone 1 (FZ1). The annual probability of fluvial (river) is less than 0.1%, ie it is outside the '1 in 1000 years' flood zone.
- 2.12 Tidal flooding: the site is 1.9 kilometres inland and removed from tidally influenced rivers.
- 2.13 Surface water flooding: occurs when excess rainwater does not infiltrate into the ground, or is not intercepted by urban drainage systems, and instead flows across the surface. The EA's surface water flood map in the 'Low Risk' scenario ('1 in 1000 years' storm event) in Appendix C shows that an overland flow route affects the southeast edge. Although this is shallow it is relatively fast flowing. This will be covered in the next section .
- 2.14 Artificial sources: flooding from reservoirs, canals and docks. The EA's reservoir flooding map (in Appendix C) shows the site as being outside of areas designated as being at risk of flooding if a reservoir were to fail. There are no docks or canals in this area.
- 2.15 Groundwater flooding: occurs when water levels in the ground rise above the surface. SBC's SFRA does not show any historical groundwater flood incidents near to the site.



# 3 Proposed Development & Drainage Strategy

- 3.1 The planning application is for 30 new private residential dwellings.
- 3.2 The site is in fluvial FZ1 and so does not need to pass the Sequential or Exception Tests. The overall risk of flooding to the site is Low, with the exception of an overland flow route along the southeast gardens.
- 3.3 The overland flow route will be managed by introducing a 450mm culvert along the east boundary . This will lead from the entrance point to the exit as shown on the drainage strategy layout in Appendix D. The headwall within the ditch at the NE corner of the site will be subject to Ordinary Watercourse Consent from the LLFA.
- 3.4 The proposed units' ground floor finished floor levels (FFLs) shall be set at least 0.15m above ambient ground levels. All housing will be at low risk of flooding, and no flood mitigation measures are required.
- 3.5 Due to the Clay geology, discharge of surface water to soakaways is considered to be unfeasible. Therefore, a site drainage strategy has been developed discharging into the re-routed ditch along northwest boundary at the north corner as shown on drawing 7267/1060B in Appendix D.
- 3.6 A series of 3 areas of porous pavings has been designed with orifices controlling the flow rate from the first 2 into the third. These orifices will be protected by a plastic mesh screen to minimise the risk of clogging.
- 3.7 As the current greenfield (Qbar) runoff rate is less than the practical minimum limit of vortex devices, namely 2.0l/s (see section 2.10 above), the offsite runoff rate will be limited to 2.0l/s in the critical 100 years +40% CC storm event. The final storage structure will be porous paving over an underground attenuation tank, whose dimensions are 222m<sup>2</sup> x 0.8m deep. This is needed as the high voids ratio will allow a relatively shallow tank of this plan area to fit into this space, ie there is insufficient area for above ground storage in this part of the site.
- 3.8 The pavings' sub-base layers will filter impurities in the water. This complies with the CIRIA guidelines.
- 3.9 Various sustainable drainage systems were considered to store the excess storm water:
  - Porous Pavings: it is proposed to use permeable paving for external drives.



- Green roofs: not practical for this development due to the proposed steep pitches of the roofs.
- Ponds/Swales: there is limited space for these features.
- Rainwater harvesting tanks: the use of rainwater harvesting tanks on a residential development where each householder would be required to maintain their own tank is not generally considered good practice or commercially viable.
- 3.10 A Micro Drainage simulation of the SW network has been carried out to demonstrate that the system will cope with the peak 1 in 100 years + 40% critical storm events. The results are contained in Appendix E.
- 3.11 The volumes in the 3 areas are summarised thus:

	Area 1	Area 2	Area 3	Tank	
Volume needed:	37.43m <sup>3</sup>	26.76m <sup>3</sup>	114.66m <sup>3</sup>	162.0m <sup>3</sup>	
Volume provided:	39.6m <sup>3</sup>	28.8m <sup>3</sup>	119.43m <sup>3</sup>	168.72m <sup>3</sup>	

- 3.12 Exceedance flows: if the outfall hydrobrake were to get clogged up, the resulting flow would be into the adjacent ditch ie away from nearby houses. Although this is not ideal, the downstream receptor is not particularly sensitive (the ditches appear to be dry a lot of the time).
- 3.13 Maintenance of the SuDS system will be the overall responsibility of the Applicant. The ongoing maintenance programme will be contracted out to a Property Maintenance company. Regular inspections of the porous pavings, tank and control manholes/orifices/hydrobrake shall be made in line with industry standards. A formal Maintenance Plan will be drafted during the next stage.
- 3.14 Foul drainage: it is proposed to discharge the development's foul water into the existing public foul sewer to the NW of the north corner see section 2.7 above. The drainage strategy layout is shown in Appendix D.
- 3.15 Permission to discharge into the public sewer by means of a Section 106 application will be sought from Southern Water, the owner of the sewerage network.



## 4 Conclusions

- 4.1 The application site has a Low Risk flood risk profile. There is an identified overland flow route along the SE boundary, which will be managed by forming a wide, shallow swale within these gardens.
- 4.2 The site's surface water flow rate will be discharged to the watercourse at the north corner at 2.0l/s in the critical storm. This runoff rate is the practical minimum limit of vortex devices (eg hydrobrakes).
- 4.3 A combination of underground tank and porous pavings' sub-bases shall hold the volume in the critical storm event (1 in 100 years + 40%). The porous pavings' fill will filter the water thus complying with CIRIA guidelines.
- 4.4 This development will not increase the flood risk, either on this site or to neighbouring properties, and so complies fully with the 2012 NPPF/2015 PPG.

- End of Report -

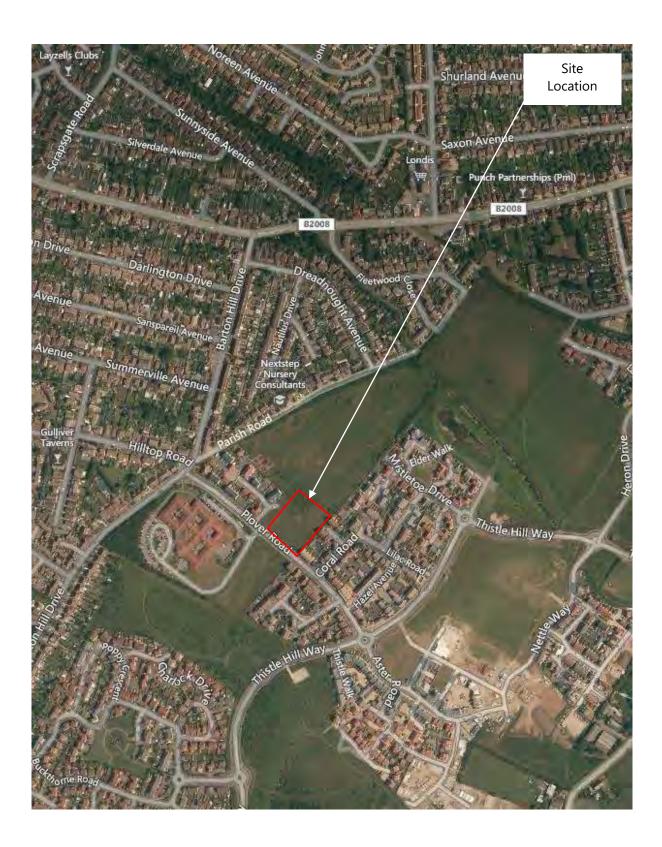


# Appendix A

# Site Location Map & Aerial Photo



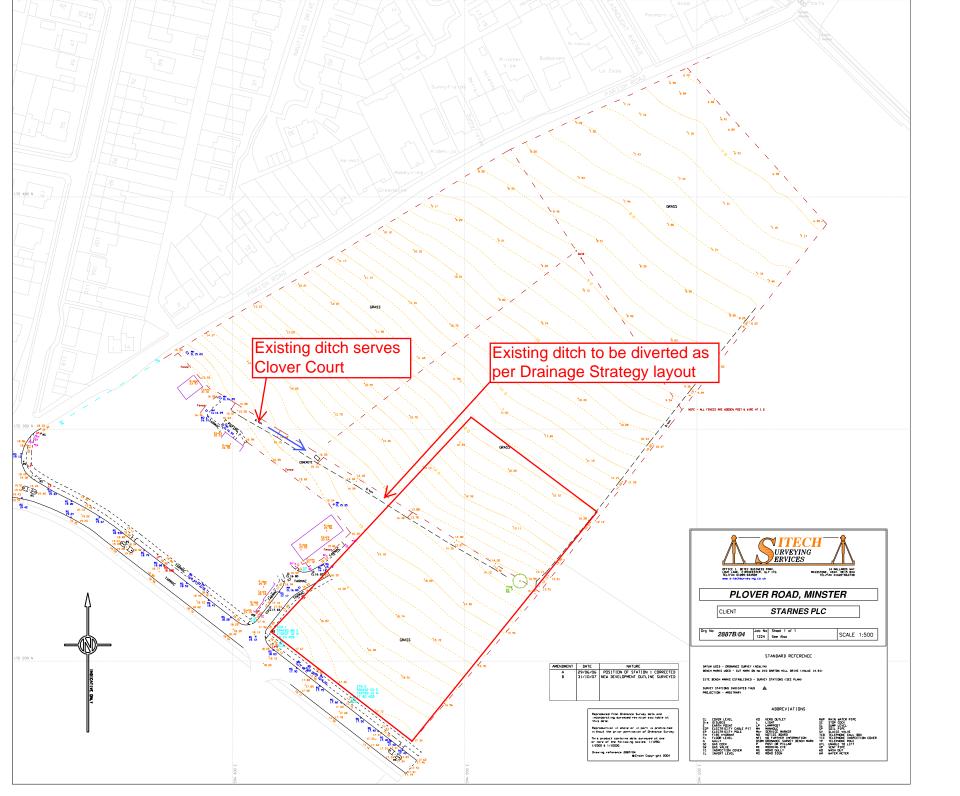


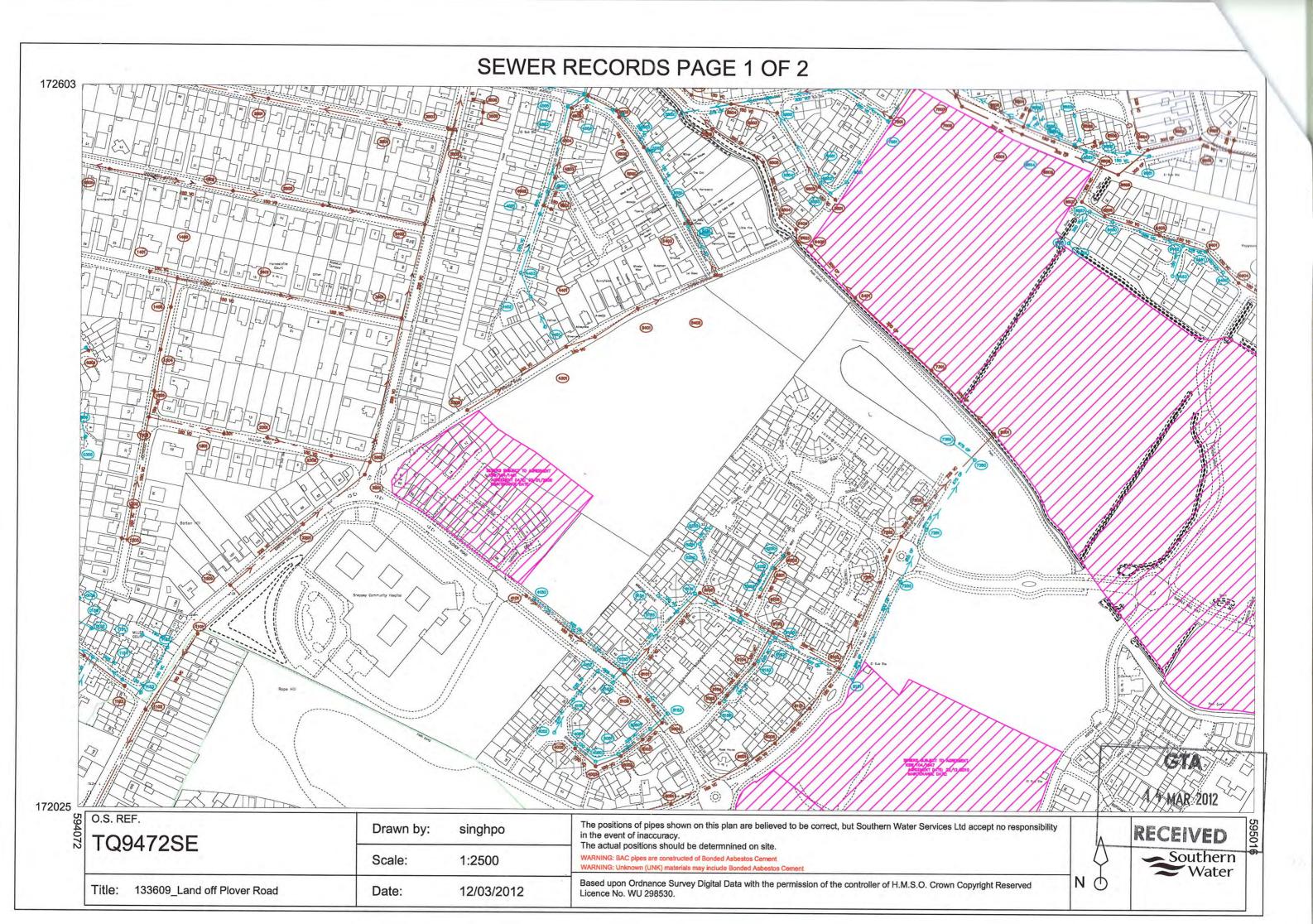




# Appendix B

Topographic Survey & Sewer Records





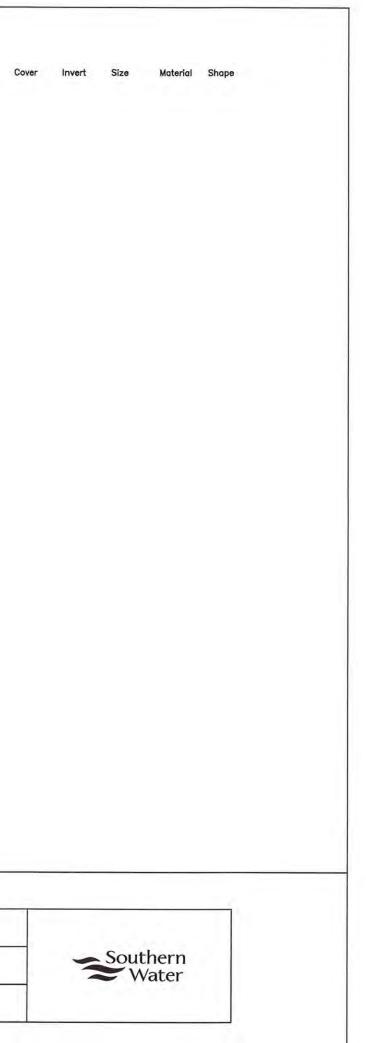
SEWER RECORDS PAGE 2 OF 2

Node	Cover	Invert	Size	Material	Shape	Node	Cover	Invert	Size	Material	Shape		Node	Cover	Invert	Size	Material	Shape	
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LINE STYLES / COLOURS MATERIALS Wistewater bestmant Warke treatment works Oddail headworks Wark Wark Wark Wark Wark Wark Wark Stankerd Stankerd Wark Wark Stankerd Wark Wark Stankerd Wark Wark Wark Stankerd Wark Alkathene Bonded Asbestos Cemen Brick (Common) Foul Syphon Sewer AX, Audurane BAC, Booder Common) BRC, Booder Common) BRC, Brick, (Engineering) CC, Concrete BRC, (Line) CC, Concrete BRC, (Line) CD, Concrete BRC, (Line) CS, Concrete (In-Sita) CS, Concrete Segments (uncoded) DI Ductie Ison CRC Glass Reinforced Deate Line) DI Ductie Ison CRC Glass Reinforced Deate Line) CRC Glass Reinforced Deate Line) CRC Glass Reinforced Deate Line) PE Phich Fors PP Polytops PF Polytops PF Polytops PF Polytops PF Polytops ST Steel ST Steel ZZZ Unknown - X ----- Foul Vacuum Main ----- Four Rising Main - Combined Drawn by: singhpo Contained Syphon Sever Micro Pumping Station Building Over Title: 133609\_Land off Plover Road SHAPES (S) - Treated Effuent Sever Catchment Section 104 Aree A Arched B Barrel C Circular E Egg H Horseshoe R Rectanguis S Square T Trapazokia U U Shape X Other H Honsethon X Other NODE REFERENCING SYSTEM 151 digit: hundred metre easting lidentifier 2nd digit: hundred metre northing identifier server type identifier 3rd digit: 0-4 = Foul/Combined 5-9 = Surface Water 4th digit: next sequential node Date: 12/03/2012 Surface Wat Private Q Decommissioned

Node



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# Appendix C

# Environment Agency Flood & Groundwater Maps



## EA's Online Flood Map for Planning (Rivers and Seas)

This site is in fluvial Flood Zone 1 (FZ1)

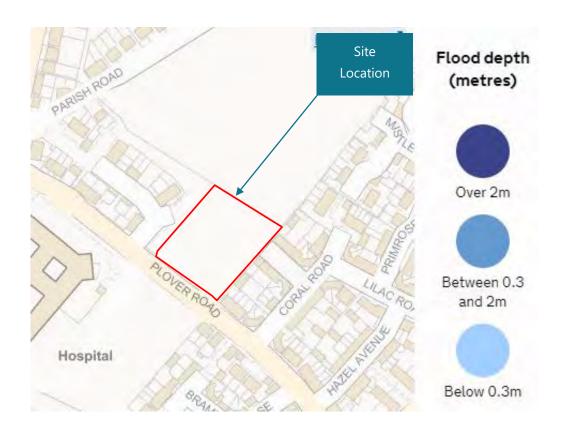




## EA's Online Surface Water Flood Depth Map in the 'Low Risk Scenario' (1 in 1000 years storm event)

A shallow overland flow route affects the southeast boundary: this will be routed through the gardens

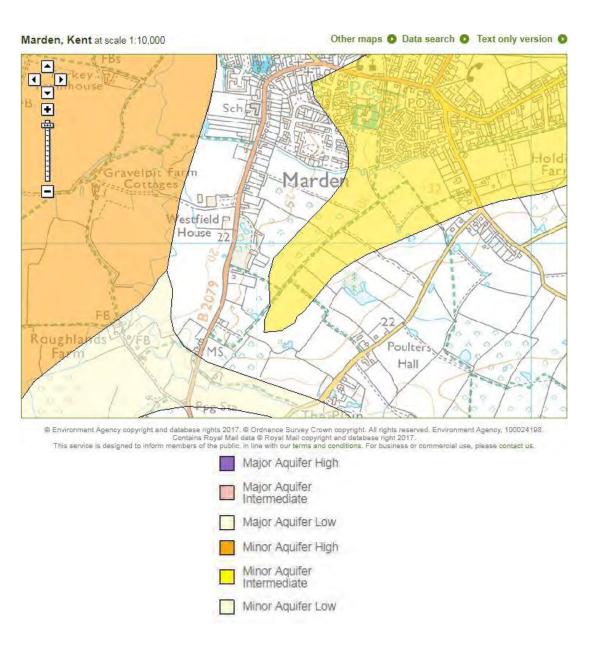




# EA's Online Risk of Flooding from Reservoirs' Map

The site is not in an area susceptible to flooding if a nearby reservoir were to fail





## Environment Agency's Groundwater Vulnerability Zone Map

The site overlies a 'Minor Aquifer - Intermediate'

# Appendix D

Proposed Scheme Drawings Including Drainage Strategy



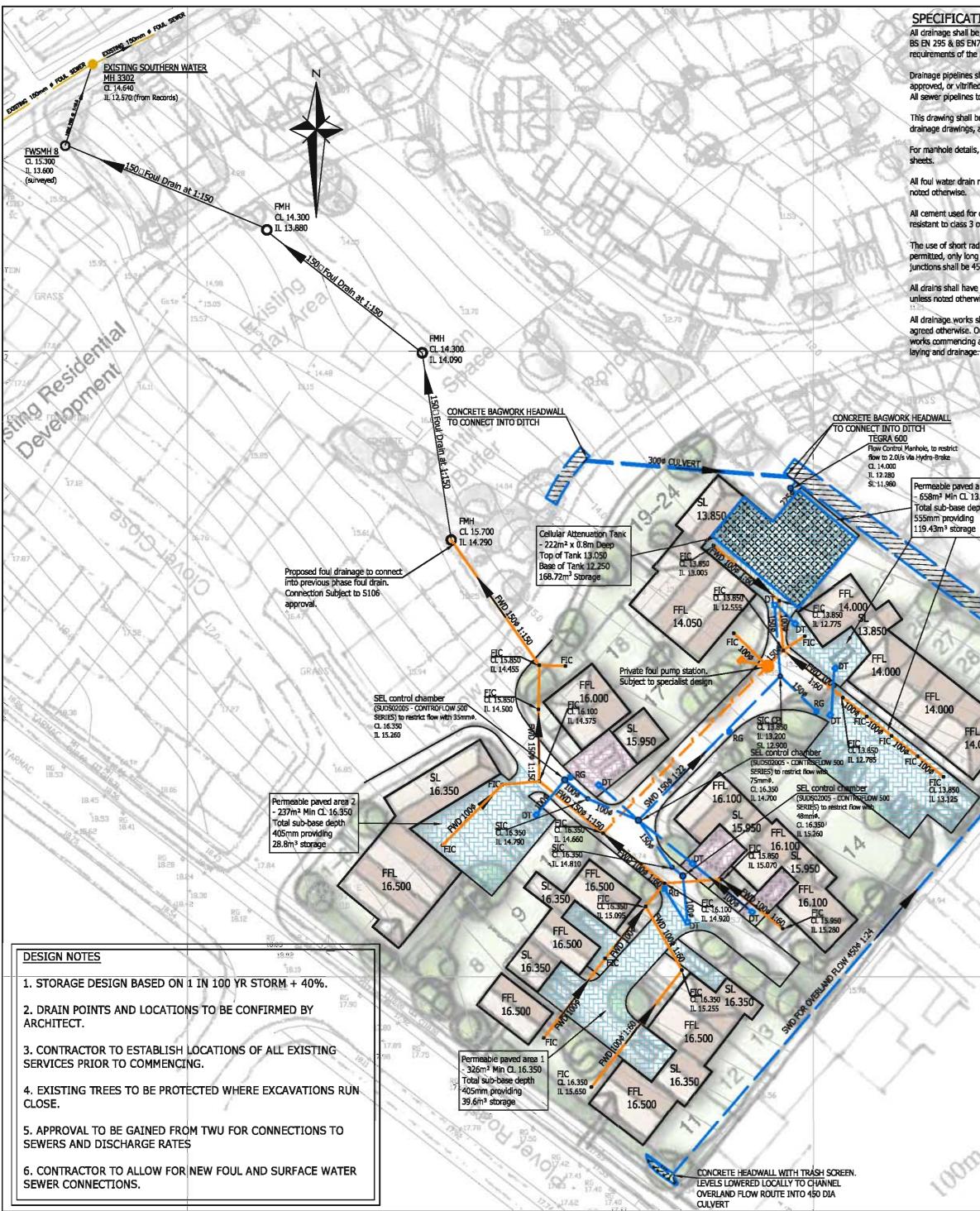
# Dalemarch (Sheppey) Ltd.



**Proposed Residential Layout** Proposed Residential Development, Land Off Plover Road, Minster Sheppey

Church Barn, Milton Manor Farm, Ashford Road, Canterbury, CT4 7PP t: 01227 456699 www.bdb-design.co.uk

eppey	Date May 2018	Drawing No.	2279B-02B					
lesidential nt, over Road,	Scale 1:1000 @A3	Drawn By SJB						
	Drawing Proposed Residential Layout							



## SPÉCIFICATION NOTES

All drainage shall be constructed and commissioned in accordance with BS EN 295 & BS EN752, Building Regulations Doc. H and any particular requirements of the Building Control Officer.

Drainage pipelines shall be in PVC-u below ground as Marley or similar approved, or vitrified clay All sewer pipelines to be VC only.

This drawing shall be read in conjunction with all other relevant drainage drawings, architectural drawings and structural drawings.

For manhole details, gully details, bedding etc, refer to GTA detail

All foul water drain runs shall have a fall of 1:40 or steeper, unless

All cement used for concrete drainage installations shall be sulphate resistant to class 3 of BRE Digest 363. (Grade ST5)

The use of short radius or 90° bends for changes in direction is not permitted, only long or medium radius 45° bends shall be used. All junctions shall be 45°.

All drains shall have granular bed and surround as class `S` bedding, unless noted otherwise.

All drainage works shall commence from the upstream end first unless agreed otherwise. Outfall level to be checked by contractor prior to any works commencing and any discrepancy identified to engineer prior to

Permeable paved area 3 658m<sup>2</sup> Min CL 13.850 Total sub-base depth 555mm providing 19.43m<sup>3</sup> storage

14.000

CONCRETE BAGWORK HEADWALL TO CONNECT INTO DITCH

## SPECIFICATION NOTES

1. ALL DRAINAGE SHALL BE CONSTRUCTED AND COMMISSIONED IN ACCORDANCE WITH BS EN 295 & BS EN752, BUILDING REGULATIONS DOC. H AND ANY PARTICULAR REQUIREMENTS OF 1. The location, size, depth and identification of existing THE BUILDING CONTROL OFFICER.

2. DRAIN BEDDING IS TO BE PROVIDED AS D200.0, D200.1 and D200.2 AS SHOWN ON THE DRAINAGE DETAILS SHEETS.

3. 'EFFECTIVE COVER' IS THE MINIMUM DEPTH OF COVER OVER THE PIPE CROWN AT ANY TIME DURING THE CONSTRUCTION PROCESS.

4. ALL CONCRETE PIPEWORK, MANHOLES AND FITTINGS SHALL BE TO BS S911 (ALL RELEVANT to works commencing. PARTS). ALL CONCRETE PIPEWORK TO BE TO HIGH STRENGTH

5. WHERE CONNECTIONS ARE TO BE MADE TO EXISTING MANHOLES/SEWERS, INVERT LEVELS, construction or the ordering of materials. PIPE SIZES & ORIENTATION SHALL BE CHECKED PRIOR TO THE COMMENCEMENT OF THE WORKS AND ANY VARIANCE REPORTED TO THE ENGINEER IMMEDIATELY.

6. WHERE PIPELINES CROSS, EACH IS TO BE SURROUNDED WITH GRADE ST4 MASS CONCRETE FOR A DISTANCE NOT LESS THAN 1m CENTRED ON THE CROSSING POINT. LENGTH OF SURROUND TO BE EXTENDED AS NECESSARY TO WITHIN 150mm OF THE NEXT NEAREST FLEXIBLE JOINTS

7. THE CONTRACTOR IS TO ENSURE THAT PROTECTIVE MEASURES ARE TAKEN TO ENSURE THAT DRAINAGE PIPEWORK AND FITTINGS ARE NOT DAMAGED BY SITE TRAFFIC PRIOR TO OVERSITE FILLING OPERATIONS BEING COMPLETED AROUND BUILDINGS.

8. ALL PRIVATE DRAINAGE PIPEWORK SHALL BE PVOL. ALL ADOPTED DRAINAGE TO BE VC. ALL 6. All drawings specifications and recommendations UNDERBUILDING DRAINS TO BE LAID AT A GRADIENT OF 1:40

9. WHERE DRAINS PASS THROUGH FOUNDATIONS OR CONNECT TO MANHOLES, FLEXIBLE PIPE services made abortive due to the client proceeding prior JOINTS ARE TO PROVIDED WITHIN 150mm OF THE FACE OF THE STRUCTURE AND WITHIN A to these approvals is considered wholly at the Clients risk. FURTHER 600mm TO FORM & ROCKER PIPE.

10. WHERE PIPES PASS THROUGH SCREEN WALLS, FOOTINGS OR RETAINING WALLS, LINTELS ARE TO BE PROVIDED.

11. WHERE PIPELINES PASS WITHIN 1m OF BUILDINGS OR WALLS THE FOUNDATIONS ARE TO BE TAKEN DOWN BELOW THE BOTTOM OF THE TRENCH

12. 450mm DIA. INSPECTION CHAMBERS (FIC/SIC) MAY BE USED: - WITH 350mm REDUCED OPENING WHERE THE DEPTH FROM COVER TO INVERT EXCEEDS 1000mm

300mm DIA. POLYPROPYLENE ACCESS CHAMBERS (FAC/SAC) MAY BE USED - WHERE THE DEPTH FROM COVER TO INVERT DOES NOT EXCEED 600mm AND WHERE THE PIPE SIZE DOES NOT EXCEED 100mm DIA.

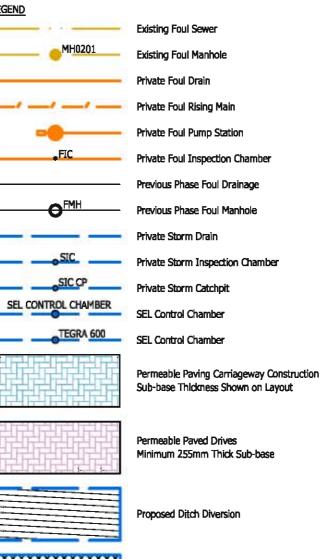
13. STEEL COVERS WITHIN PROPERTY BOUNDARIES SHALL BE: (UNLESS NOTED ON DRAWING OR MANHOLE SCHEDULE) -ON PRIVATE DRIVEWAYS: FACTA GRADE B (BS EN ISO 1461: 1999) -ON PRIVATE PATHWAYS, VERGES OR ON GARDENS: FACTA GRADE A (BS EN ISO 1461: 1999)

DUCTILE IRON COVERS OUTSIDE PROPERTY BOUNDARIES SHALL BE: (UNLESS NOTED ON DRAWING OR MANHOLE SCHEDULE) -ON ACCESS ROADS AND CAR PARKS: GRADE D400 (BS EN 124:1994) -ON SHARED PATHWAYS, VERGES: GRADE A15 (BS EN 124:1994)

14. COVER LEVELS SHOWN 'CL' AND INVERT LEVELS SHOWN 'IL' ARE IN METRES ABOVE ORDNANCE DATUM.

15. ALL DRAINS TO BE 100mm DIAMETER UNLESS NOTED OTHERWISE

16. ALL DRAINS MARKED 'FWS' OR 'SWS' ARE PROPOSED ADOPTED SEWERS AND ARE TO BE CONSTRUCTED IN ACCORDANCE WITH 'SEWERS FOR ADOPTION, 7TH EDITION'



Cellular Attenuation Tank Located Beneath Permeable Paved Area

## GENERAL NOTES

services that may be shown or referred to on this drawing have been assessed from non intrusive observations, record drawings or the like. The contractor shall safely carry out intrusive investigations, trial holes or soundings prior to commencing work to satisfy himself that it is safe to proceed and that the assessments are accurate. any discrepancies shall be notified to gta prior

2. Tender or billing drawings shall not be used for

3. Do not scale. All dimensions and levels to be site confirmed.

4. This drawing shall be read in conjunction with all relevant architects, consultants drawings and specifications, together with H&S plan requirements

S. Copyright : This drawing must not be copied, amended nor reproduced without the prior written agreement of ata

made by gta are subject to Local Authority and other relevant Statutory Authorities approval. Any works or gta hold no responsibility for resulting abortive works or costs.

Overland flow route pipe added 13/09/18 Flow Restriction Adjusted 30/04/18 I MR 22/03/18 Initial Issue MR Date Dsn Chk Statu PRELIMINARY Client DALEMARCH (SHEPPEY) LTD Architect Project LAND AT PLOVER ROAD,

# MINSTER, ME12 3BT

PROPOSED DRAINAGE STRATEGY

MARCH 2018

lients Re

7267

1:500

•gtaCivils Gloucester House, 66a Church Walk, Burgess Hill, West Sussex, RH15 9AS Tel.01444 871444 Web: www.gtacivils.co.uk

7267/1060



Appendix E

Drainage Calculation Sheets

GTA Civils Ltd		Page 1
Gloucester House		
66a Church Walk		L
Burgess Hill RH15 9AS		Micco
Date 18/04/2018 09:40	Designed by jpakenham	Drainage
File	Checked by	Diamaye
Micro Drainage	Source Control 2016.1.1	

## ICP SUDS Mean Annual Flood

Input

Return Period (years)	100	Soil	0.450
Area (ha)	0.321	Urban	0.000
SAAR (mm)	565	Region Number	Region 7

## Results 1/s

QBAR Rural 1.1 QBAR Urban 1.1 Q100 years 3.5

Q1 year 0.9 Q30 years 2.5 Q100 years 3.5

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Burgess Hill RH15 9AS		Micro		
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Micro Drainage	Network 2016.1.1			

## <u>Time Area Diagram for Storm</u>

Time	Area	Time	Area
(mins)	(ha)	(mins)	(ha)
0-4	0.272	4-8	0.121

Total Area Contributing (ha) = 0.393

Total Pipe Volume (m³) = 1.614

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Micro Drainage	Network 2016.1.1	

		<u>SIURM</u>		<u>r desi</u>	<u>y u v</u>	<u>the</u> r	10011.	Ieu Ka		al M		
				Networ	k Desi	gn Ta	able :	for St	Corm			
				« – Ind	dicates	pipe	capaci	lty < f	low			
PN	Length	Fall	Slope	I.Area	T.E.	Ba	se	k	HYD	DIA	Section Type	Auto
	(m)	(m)	(1:X)	(ha)	(mins)	Flow	(l/s)	(mm)	SECT	(mm)		Design
S1.000	7.157	0.490	14.6	0.100	4.00		0.0	0.600	0	100	Pipe/Conduit	•
S1.001	2.200	0.450	4.9	0.000	0.00		0.0	0.600	0	100	Pipe/Conduit	ē
S1.002	9.250	0.110	84.1	0.000	0.00		0.0	0.600	0	150	Pipe/Conduit	ě
S2.000	10.793	0.800	13.5	0.036	4.00		0.0	0.600	0	100	Pipe/Conduit	•
s3.000	6.910	0.490	14.1	0.067	4.00		0.0	0.600	0	100	Pipe/Conduit	8
				Ne	twork	Resu	lts T	able				

PN	Rain	T.C.	US/IL	Σ I.Area	Σ Bas	Σ Base		Add Flow	Vel	Cap	Flow	
	(mm/hr)	(mins)	(m)	(ha)	Flow (1	/s)	(l/s)	(1/s)	(m/s)	(l/s)	(l/s)	
S1.000	50.00	4.06	15.750	0.100		0.0	0.0	0.0	2.03	16.0	13.5	
S1.001	50.00	4.07	15.260	0.100		0.0	0.0	0.0	3.52	27.7	13.5	
S1.002	50.00	4.21	14.810	0.100		0.0	0.0	0.0	1.10	19.4	13.5	
S2.000	50.00	4.09	15.500	0.036		0.0	0.0	0.0	2.11	16.6	4.9	
S3.000	50.00	4.06	15.750	0.067		0.0	0.0	0.0	2.07	16.2	9.1	

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Micro Drainage	Network 2016.1.1	

		STORM	SEWE	r desi	GN by	the Modi	fied R	ation	al M	ethod	
				Networ	<u>k Desi</u>	<u>gn Table</u>	for S	<u>torm</u>			
PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)		Base Flow (l/s	k ;) (mm)	HYD SECT		Section Type	Auto Design
S3.001	4.746	0.420	11.3	0.000	0.00	0.	0 0.600	0	100	Pipe/Conduit	0
S3.002	8.770	0.090	97.4	0.000	0.00	0.	0 0.600	0	150	Pipe/Conduit	ē
S4.000	8.102	0.800	10.1	0.021	4.00	0.	0 0.600	0	100	Pipe/Conduit	•
s1.003	32.342	1.500	21.6	0.000	0.00	0.	0 0.600	0	150	Pipe/Conduit	•
S1.004	11.141	0.900	12.4	0.000	0.00	0.	0 0.600	0	150	Pipe/Conduit	ě
s5.000	8.886	0.000	0.0	0.169	4.00	0.	0 0.600	0	100	Pipe/Conduit	•

#### <u>Network Results Table</u>

PI	N	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)		Add Flow (l/s)		Cap (1/s)	Flow (1/s)
S3.(	001	50.00	4.09	15.260	0.067	0.0	0.0	0.0	2.31	18.2	9.1
S3.(	002	50.00	4.23	14.790	0.067	0.0	0.0	0.0	1.02	18.0	9.1
S4.(	000	50.00	4.06	15.500	0.021	0.0	0.0	0.0	2.44	19.2	2.8
S1.(	003	50.00	4.48	14.700	0.224	0.0	0.0	0.0	2.18	38.5	30.3
S1.(	004	50.00	4.55	13.200	0.224	0.0	0.0	0.0	2.88	50.9	30.3
S5.(	000	50.00	6.13	12.300	0.169	0.0	0.0	0.0	0.07	0.5«	22.9
				©	1982-201	6 XP Solu	tions				

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Micro Drainage	Network 2016.1.1	I

		<u>STORI</u>	<u>4 sewi</u>	ER DES	IGN by	the N	<u>lodif:</u>	led Ra	tion	al M	ethod	<u>.</u>	
Network Design Table for Storm													
PN 1	Length (m)		-	a I.Area (ha)	a T.E. (mins)		se (1/s)		HYD SECT		Secti	on Type	e Auto Design
					0.00			0.600 0.600			-	Conduit Conduit	
				N	letwork	Resu	<u>lts T</u>	<u>able</u>					
PN	Rai (mm/		<b>F.C.</b> mins)	US/IL (m)	Σ I.Area (ha)			Foul (1/s)			Vel (m/s)	Cap (1/s)	
S1.00 S1.00		.00		12.300 12.280	0.393 0.393		0.0					65.9 96.1	

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Micro Drainage	Network 2016.1.1	

MH Name	MH CL (m)	MH Depth (m)	Conr	MH nection	MH Diam.,L*W (mm)	PN	Pipe Out Invert Level (m)	Diameter (mm)	PN	Pipes In Invert Level (m)	Diameter (mm)	Backdrop (mm)
S1	16.350	0.600	Open	Manhole	1200	s1.000	15.750	100				
s2	16.500	1.240	Open	Manhole	1200	S1.001	15.260	100	S1.000	15.260	100	
S3	16.350	1.540	Open	Manhole	1200	S1.002	14.810	150	S1.001	14.810	100	
S4	15.950	0.450	Open	Manhole	1200	S2.000	15.500	100				
S5	16.350	0.600	Open	Manhole	1200	S3.000	15.750	100				
S6	16.500	1.240	Open	Manhole	1200	S3.001	15.260	100	S3.000	15.260	100	
s7	16.350	1.560	Open	Manhole	1200	S3.002	14.790	150	S3.001	14.840	100	
S8	15.950	0.450	Open	Manhole	1200	S4.000	15.500	100				
S4	16.500	1.800	Open	Manhole	1200	S1.003	14.700	150	S1.002	14.700	150	
									S2.000	14.700	100	
									S3.002	14.700	150	
									S4.000	14.700	100	
s5	14.000	0.800	Open	Manhole	1200	S1.004	13.200	150	S1.003	13.200	150	
S12	13.850	1.550	Open	Manhole	1200	S5.000	12.300	100				
S6	13.850	1.550	Open	Manhole	1200	S1.005	12.300	225	S1.004	12.300	150	
									S5.000	12.300	100	
s7	14.000	1.720	Open	Manhole	1200	S1.006	12.280	300	S1.005	12.280	225	
S	14.000	1.730	Open	Manhole	0		OUTFALL		S1.006	12.270	300	

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Micro Drainage	Network 2016.1.1	

#### PIPELINE SCHEDULES for Storm

## <u>Upstream Manhole</u>

Hyd	Diam	MH	C.Level	I.Level	D.Depth	MH	MH DIAM., L*W
Sect	(mm)	Name	(m)	(m)	(m)	Connection	(mm)
0	100	S1	16.350	15.750	0.500	Open Manhole	1200
0	100	s2	16.500	15.260	1.140	Open Manhole	1200
0	150	S3	16.350	14.810	1.390	Open Manhole	1200
0	100	S4	15.950	15.500	0.350	Open Manhole	1200
0	100	s5	16.350	15.750	0.500	Open Manhole	1200
0	100	S6	16.500	15.260	1.140	Open Manhole	1200
0	150	S7	16.350	14.790	1.410	Open Manhole	1200
	Sect 0 0 0 0	Sect (mm) o 100 o 100 o 150 o 100 o 100 o 100 o 100	Sect     (mm)     Name       0     100     S1       0     100     S2       0     150     S3       0     100     S4       0     100     S5       0     100     S5       0     100     S5	Sect     (mm)     Name     (m)       0     100     S1     16.350       0     100     S2     16.500       0     150     S3     16.350       0     100     S4     15.950       0     100     S5     16.350       0     100     S5     16.350       0     100     S5     16.350       0     100     S5     16.350	Sect     (mm)     Name     (m)     (m)       0     100     S1     16.350     15.750       0     100     S2     16.500     15.260       0     150     S3     16.350     14.810       0     100     S4     15.950     15.500       0     100     S5     16.350     15.750       0     100     S5     16.350     15.750       0     100     S6     16.500     15.260	Sect (mm)     Name     (m)     (m)     (m)       0     100     S1     16.350     15.750     0.500       0     100     S2     16.500     15.260     1.140       0     150     S3     16.350     14.810     1.390       0     100     S4     15.950     15.500     0.350       0     100     S5     16.350     15.750     0.500       0     100     S5     16.350     15.750     0.500       0     100     S6     16.500     15.260     1.140	Sect     (mm)     Name     (m)     (m)     (m)     Connection       o     100     S1     16.350     15.750     0.500     Open Manhole       o     100     S2     16.500     15.260     1.140     Open Manhole       o     150     S3     16.350     15.500     0.350     Open Manhole       o     100     S4     15.950     15.500     0.350     Open Manhole       o     100     S5     16.350     15.750     0.500     Open Manhole       o     100     S5     16.350     15.750     0.500     Open Manhole       o     100     S5     16.500     15.260     1.140     Open Manhole

#### <u>Downstream Manhole</u>

PN	Length	Slope	MH	C.Level	I.Level	D.Depth	MH	MH DIAM., L*W				
	(m)	(1:X)	Name	(m)	(m)	(m)	Connection	(mm)				
S1.000	7.157	14.6	s2	16.500	15.260	1.140	Open Manhole	1200				
S1.001	2.200	4.9	s3	16.350	14.810	1.440	Open Manhole	1200				
S1.002	9.250	84.1	S4	16.500	14.700	1.650	Open Manhole	1200				
S2.000	10.793	13.5	S4	16.500	14.700	1.700	Open Manhole	1200				
s3.000	6.910	14.1	S6	16.500	15.260	1.140	Open Manhole	1200				
S3.001	4.746	11.3	s7	16.350	14.840	1.410	Open Manhole	1200				
S3.002	8.770	97.4	S4	16.500	14.700	1.650	Open Manhole	1200				
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66a Church Walk	Storm Network Design	L.
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Micro Drainage	Network 2016.1.1	

#### PIPELINE SCHEDULES for Storm

## <u>Upstream Manhole</u>

PN	Hyd Sect		MH Name	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
S4.000	0	100	S8	15.950	15.500	0.350	Open Manhole	1200
S1.003 S1.004	-	150 150		16.500 14.000	14.700 13.200		Open Manhole Open Manhole	1200 1200
S5.000	0	100	S12	13.850	12.300	1.450	Open Manhole	1200
S1.005	0	225	S6	13.850	12.300	1.325	Open Manhole	1200

#### <u>Downstream Manhole</u>

	PN	Length (m)	Slope (1:X)			I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)	
:	s4.000	8.102	10.1	S4	16.500	14.700	1.700	Open Manhole	1200	
		32.342 11.141			14.000 13.850			Open Manhole Open Manhole	1200 1200	
:	\$5.000	8.886	0.0	S6	13.850	12.300	1.450	Open Manhole	1200	
:	s1.005	1.250	62.5	S7	14.000	12.280	1.495	Open Manhole	1200	
				C	01982-20	)16 XP 3	Solutio	ns		

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#### PIPELINE SCHEDULES for Storm

## <u>Upstream Manhole</u>

PN	-	Diam (mm)		C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
S1.006	0	300	s7	14.000	12.280	1.420	Open Manhole	1200

#### Downstream Manhole

PN	Length	Slope	MH	C.Level	I.Level	D.Depth	MH	MH DIAM.,	L*₩	
	(m)	(1:X)	Name	(m)	(m)	(m)	Connection	(mm)		
S1.006	1.333	133.3	S	14.000	12,270	1,430	Open Manhole		0	

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Micro Drainage	Network 2016.1.1	

#### <u>Area Summary for Storm</u>

Pipe	PIMP	PIMP	PIMP	Gross	Imp.	Pipe Total
Number	Туре	Name	(%)	Area (ha)	Area (ha)	(ha)
1.000	_	_	100	0.100	0.100	0.100
1.000	_	_	100	0.000	0.000	0.000
1.002	-	-	100	0.000	0.000	0.000
2.000	-	-	100	0.036	0.036	0.036
3.000	-	-	100	0.067	0.067	0.067
3.001	-	-	100	0.000	0.000	0.000
3.002	-	-	100	0.000	0.000	0.000
4.000	-	-	100	0.021	0.021	0.021
1.003	-	-	100	0.000	0.000	0.000
1.004	-	-	100	0.000	0.000	0.000
5.000	-	-	100	0.169	0.169	0.169
1.005	-	-	100	0.000	0.000	0.000
1.006	-	-	100	0.000	0.000	0.000
				Total	Total	Total
				0.393	0.393	0.393

Free Flowing Outfall Details for Storm

Out	tfall	Outfall	c.	Level	I.	Level		Min	D,L	W
Pipe	Number	Name		(m)		(m)	I.	Level	(mm)	(mm)
								(m)		
	S1.006	S		14.000		12.270		14.000	0	0

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Micro Drainage	Network 2016.1.1	L

<u>Simulation</u>	Criteria	for	Storm
-------------------	----------	-----	-------

Volumetric Runoff Coeff 0.750 Manhole Headloss Coeff (Global) 0.500	Inlet Coeffiecient 0.800
Areal Reduction Factor 1.000 Foul Sewage per hectare (1/s) 0.000 Flow per Pe	rson per Day (l/per/day) 0.000
Hot Start (mins) 0 Additional Flow - % of Total Flow 0.000	Run Time (mins) 60
Hot Start Level (mm) 0 MADD Factor * 10m³/ha Storage 2.000	Output Interval (mins) 1
Number of Input Hydrographs 0 Number of Offline Controls 0 Number of	5
Number of Online Controls 4 Number of Storage Structures 5 Number of 1	Real Time Controls 0
<u>Synthetic Rainfall Details</u>	
Rainfall Model FSR M5-60 (mm) 20.900	
Return Period (years) 1 Ratio R 0.392	
Region England and Wales Profile Type Summer Storm Dura	ation (mins) 30

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Micro Drainage	6.1.1				
	<u>Online Controls</u>	for Storm			
<u>Orifice Ma</u>	nhole: S2, DS/PN: S	51.001, Volume (m³):	1.4		
Diameter (m) 0.0	48 Discharge Coefficie	nt 0.600 Invert Level (m	) 15.260		
Orifice Ma	nhole: S6, DS/PN: S	53.001, Volume (m³):	1.4		
Diameter (m) 0.0	35 Discharge Coefficie	nt 0.600 Invert Level (m	) 15.260		
Orifice Ma	nhole: S4, DS/PN: S	51.003, Volume (m³):	2.4		
Diameter (m) 0.0	75 Discharge Coefficie	nt 0.600 Invert Level (m	) 14.700		
<u>Hydro-Brake® Opti</u>	imum Manhole: S7, D	S/PN: S1.006, Volume	(m <sup>3</sup> ): 1.9		
Design Head (m) Design Flow (l/s) Flush-Flo™		Diame Invert 1 Minimum Outlet Pipe Diame			
Objective Minir Application	nise upstream storage Surface	Suggested Manhole Diame	eter (mm) 1200		
Control Points E	lead (m) Flow (l/s)	Control Points	Head (m) Flow (l/s)		
	1.573 2.0 0.266 1.5 Mea	Kick-Flo® an Flow over Head Range			
The hydrological calculations have been based on	the Head/Discharge rel	ationship for the Hydro-	Brake® Optimum as spec	ified. Should	
	©1982-2016 XP	Solutions			

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## Hydro-Brake® Optimum Manhole: S7, DS/PN: S1.006, Volume (m<sup>3</sup>): 1.9

another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)										
0.100	1.3	0.600	1.3	1.600	2.0	2.600	2.5	5.000	3.4	7.500	4.1
0.200	1.5	0.800	1.5	1.800	2.1	3.000	2.7	5.500	3.6	8.000	4.2
0.300	1.5	1.000	1.6	2.000	2.2	3.500	2.9	6.000	3.7	8.500	4.4
0.400	1.5	1.200	1.8	2.200	2.3	4.000	3.1	6.500	3.9	9.000	4.5
0.500	1.3	1.400	1.9	2.400	2.4	4.500	3.2	7.000	4.0	9.500	4.6

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Micro Drainage	Network 2016.1.1	

#### Storage Structures for Storm

#### Porous Car Park Manhole: S1, DS/PN: S1.000

0.0	Slope (1:X)	0.30	sity	Poros	0.00000	Infiltration Coefficient Base (m/hr)
5	Depression Storage (mm)	15.750	(m)	Invert Level	1000	Membrane Percolation (mm/hr)
3	Evaporation (mm/day)	5.0	(m)	Width	90.3	Max Percolation (l/s)
0	Membrane Depth (mm)	65.0	(m)	Length	2.0	Safety Factor

#### Porous Car Park Manhole: S4, DS/PN: S2.000

Infiltration Coefficient Base (m/hr)	0.00000	Poros	ity 0.30	Slope (1:X) 0.0
Membrane Percolation (mm/hr)	1000	Invert Level	(m) 15.500	Depression Storage (mm) 5
Max Percolation (1/s)	23.9	Width	(m) 4.1	Evaporation (mm/day) 3
Safety Factor	2.0	Length	(m) 21.0	Membrane Depth (mm) 0

#### Porous Car Park Manhole: S5, DS/PN: S3.000

Infiltration Coefficient Base (m/hr)	0.00000	Poros	ity	0.30	Slope (1:X)	0.0
Membrane Percolation (mm/hr)	1000	Invert Level	(m)	15.750	Depression Storage (mm)	5
Max Percolation (l/s)	65.7	Width	(m)	12.0	Evaporation (mm/day)	3
Safety Factor	2.0	Length	(m)	19.7	Membrane Depth (mm)	0

#### Porous Car Park Manhole: S8, DS/PN: S4.000

Infiltration Coefficient Base (m/hr)0.00000Safety Factor2.0Width (m)7.2Membrane Percolation (mm/hr)1000Porosity0.30Length (m)9.0Max Percolation (1/s)18.0Invert Level (m)15.500Slope (1:X)0.0

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Gloucester House	Plover Road, Minster	
66a Church Walk	Storm Network Design	4
Burgess Hill RH15 9AS		Micro
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File 180430_Network_Calc.mdx	Checked by JP	Drainage
Micro Drainage	Network 2016.1.1	I

#### Porous Car Park Manhole: S8, DS/PN: S4.000

Depression Storage (mm) 5 Evaporation (mm/day) 3 Membrane Depth (mm) 0

Complex Manhole: S12, DS/PN: S5.000

#### <u>Cellular Storage</u>

Invert Level (m) 12.300 Infiltration Coefficient Side (m/hr) 0.00000 Porosity 0.95 Infiltration Coefficient Base (m/hr) 0.00000 Safety Factor 2.0

Depth (m) Area (m<sup>2</sup>) Inf. Area (m<sup>2</sup>) Depth (m) Area (m<sup>2</sup>) Inf. Area (m<sup>2</sup>) Depth (m) Area (m<sup>2</sup>) Inf. Area (m<sup>2</sup>)

0.000 217.0 217.0 0.800 217.0 264.2 0.900 0.0 264.2

#### <u>Porous Car Park</u>

Infiltration Coefficient Base (m/hr)	0.00000	Poros	sity	0.30	Slope (1:X) 0.0
Membrane Percolation (mm/hr)	1000	Invert Level	(m)	13.100	Depression Storage (mm) 5
Max Percolation (1/s)	182.8	Width	(m)	7.0	Evaporation (mm/day) 3
Safety Factor	2.0	Length	(m)	94.0	Membrane Depth (mm) 0

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Gloucester House	]	Plover Road, Minste	r	
66a Church Walk	\$	Storm Network Desig	n	4
Burgess Hill RH15 9AS				Mirro
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File 180430_Network_Calc.mdx	(	Checked by JP		Diamaye
Micro Drainage	1	Network 2016.1.1		l
<u>1 year Return P</u>	eriod Summary of Cr		Maximum Level (Ran)	<u>&lt; 1) for Storm</u>
Areal Reduction Factor Hot Start (mins) Hot Start Level (mm)	1.000 Manhole Headlos 0 Foul Sewage p 0 Additional Flow -	per hectare (1/s) 0.000 - % of Total Flow 0.000	) In ) Flow per Person per	Let Coeffiecient 0.800 Day (l/per/day) 0.000
-	nt Hydrographs 0 Numb Aline Controls 4 Number			5
Ra	infall Model	<u>thetic Rainfall Details</u> FSR M5-60 (mm) 20. nd Wales Ratio R 0.	400 Cv (Summer) 0.750	
Margin for	Flood Risk Warning (mm Analysis Timeste DTS Statu	ep 2.5 Second Increment		Status ON Status ON
	) (years)	80, 240, 360, 480, 600		Winter 0, 2880, 4320, 0, 8640, 10080 1, 30, 100 0, 0, 40
US/MH PN Name	US/CI Event (m)	-	olume Flow / Overflow	Pipe W Maximum Flow Vol (m³) (l/s) Status
S1.000 S1 60 minute 1	year Winter I+0% 16.35	0 15.795 -0.055	0.000 0.32	4.432 4.6 OK
	©198	32-2016 XP Solution	S	

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Gloucester House	Plover Road, Minster	
66a Church Walk	Storm Network Design	L.
Burgess Hill RH15 9AS		Micro
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File 180430_Network_Calc.mdx	Checked by JP	Drainage
Micro Drainage	Network 2016.1.1	

## 1 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name	Event	US/CL (m)	Water Level (m)	Surcharged Depth (m)		Flow / Cap.	Overflow (1/s)	Maximum Vol (m <sup>3</sup> )	Pipe Flow (l/s)	Status
S1.001	s2	60 minute 1 year Winter I	+0% 16.500	15.769	0.409	0.000	0.18		0.613	3.3	SURCHARGED
S1.002	s3	60 minute 1 year Winter I	+0% 16.350	15.180	0.220	0.000	0.21		0.419	3.6	SURCHARGED
S2.000	S4	60 minute 1 year Winter I	+0% 15.950	15.527	-0.073	0.000	0.16		0.721	2.5	OK
S3.000	S5	60 minute 1 year Winter I	+0% 16.350	15.791	-0.059	0.000	0.22		2.979	3.3	OK
S3.001	S6	60 minute 1 year Winter I	+0% 16.500	15.779	0.419	0.000	0.11		0.623	1.8	SURCHARGED
S3.002	s7	60 minute 1 year Winter I	+0% 16.350	15.175	0.235	0.000	0.13		0.448	2.0	SURCHARGED
S4.000	S8	60 minute 1 year Winter I	+0% 15.950	15.519	-0.081	0.000	0.08		0.392	1.5	OK
S1.003	S4	60 minute 1 year Winter I	+0% 16.500	15.169	0.319	0.000	0.21		0.868	7.7	SURCHARGED
S1.004	S5	60 minute 1 year Winter I	+0% 14.000	13.241	-0.109	0.000	0.17		0.045	7.7	OK
S5.000	S12	720 minute 1 year Winter I	+0% 13.850	12.530	0.130	0.000	0.85		47.752	2.2	SURCHARGED
S1.005	S6	180 minute 1 year Winter I	+0% 13.850	12.539	0.014	0.000	0.06		0.356	1.7	SURCHARGED
S1.006	s7	180 minute 1 year Winter I	+0% 14.000	12.539	-0.041	0.000	0.03		0.291	1.5	OK

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Gloucester Hous	е		Plover Road,	Minster	
66a Church Walk	:		Storm Network	Design	L.
Burgess Hill R	H15 9AS				Micco
Date 30/04/2018	15:57		Designed by L	Г	Desinance
File 180430_Net	work_Cal	c.mdx	Checked by JP		Diamage
licro Drainage			Network 2016.	1.1	l
	<u>30 year</u>	<u>r Return Period Summar</u>	y of Critical Resul <sup>.</sup> Simulation Crit	-	Rank 1) for Storm
		ion Factor 1.000 Manhole art (mins) 0 Foul Level (mm) 0 Additiona	<u> </u>		
		ber of Input Hydrographs ( Number of Online Controls (			
		Rainfall Model Region En		Details mm) 20.400 Cv (Summer) 0 o R 0.380 Cv (Winter) 0	
			-	10.0 DV Crement (Extended) Inerti ON	'D Status ON a Status ON
	Retur	Profile(s) Duration(s) (mins) 60 rn Period(s) (years) Climate Change (%)	120, 180, 240, 360, 4	80, 600, 720, 960, 1440, 2 5760, <sup>2</sup>	Winter 2160, 2880, 4320, 7200, 8640, 10080 1, 30, 100 0, 0, 40
PN	US/MH Name	Event	Water Surchar US/CL Level Depth (m) (m) (m)	Volume Flow / Overfl	Pipe ow Maximum Flow Vol (m <sup>3</sup> ) (l/s) Status
S1.000	S1 60 :	minute 30 year Winter I+0%	16.350 15.917 0.	0.000 0.38	16.506 5.5 SURCHARGED

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Gloucester House	Plover Road, Minster	
66a Church Walk	Storm Network Design	L.
Burgess Hill RH15 9AS		Micro
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Micro Drainage	Network 2016.1.1	

## 30 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name			E	vent			US/CL (m)	Water Level (m)	Surcharged Depth (m)		Flow / Cap.	Overflow (1/s)	Maximum Vol (m³)	Pipe Flow (l/s)	Status
S1.001	S2	60	minute	30	year	Winter	I+0%	16.500	15.896	0.536	0.000	0.20		0.760	3.7	SURCHARGED
S1.002	S3	60	minute	30	year	Winter	I+0%	16.350	15.534	0.574	0.000	0.24		0.821	4.1	SURCHARGED
S2.000	S4	60	minute	30	year	Winter	I+0%	15.950	15.573	-0.027	0.000	0.37		1.969	5.8	OK
S3.000	s5	60	minute	30	year	Winter	I+0%	16.350	15.910	0.060	0.000	0.29		11.533	4.2	SURCHARGED
S3.001	S6	60	minute	30	year	Winter	I+0%	16.500	15.898	0.538	0.000	0.13		0.760	2.0	SURCHARGED
S3.002	s7	60	minute	30	year	Winter	I+0%	16.350	15.530	0.590	0.000	0.15		0.859	2.4	SURCHARGED
S4.000	S8	60	minute	30	year	Winter	I+0%	15.950	15.541	-0.059	0.000	0.21		0.845	3.6	OK
S1.003	S4	60	minute	30	year	Winter	I+0%	16.500	15.525	0.675	0.000	0.28		1.327	10.4	SURCHARGED
S1.004	S5	60	minute	30	year	Winter	I+0%	14.000	13.248	-0.102	0.000	0.23		0.054	10.4	OK
S5.000	S12	720	minute	30	year	Winter	I+0%	13.850	12.959	0.559	0.000	0.70		136.569	1.8	SURCHARGED
S1.005	S6	720	minute	30	year	Winter	I+0%	13.850	12.956	0.431	0.000	0.05		0.909	1.6	SURCHARGED
S1.006	S7	720	minute	30	year	Winter	I+0%	14.000	12.956	0.376	0.000	0.03		0.763	1.5	SURCHARGED

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Gloucester House		Plover Road, Minster						
66a Church Walk		Storm Network Design	Storm Network Design					
Burgess Hill RH15 9AS				Mirco				
Date 30/04/2018 15:57		Designed by LT		Desipado				
File 180430_Network_Cal	Lc.mdx	Checked by JP		Diamage				
Micro Drainage		Network 2016.1.1						
<u>100 yea</u>	ar Return Period Summary	y of Critical Results by Maxi	mum Level (Rank 1) for Sto	orm.				
Hot St	art (mins) 0 Foul S	Simulation Criteria Headloss Coeff (Global) 0.500 ewage per hectare (1/s) 0.000 Flow - % of Total Flow 0.000 Flow	Inlet Coefficcient	z 0.800				
		Number of Offline Controls 0 Number of Storage Structures 5 Num						
	Rainfall Model Region Eng	<u>Synthetic Rainfall Details</u> FSR M5-60 (mm) 20.400 ( land and Wales Ratio R 0.380 (						
	-	ing (mm) Timestep 2.5 Second Increment (Ext S Status	10.0 DVD Status ON ended) Inertia Status ON ON					
Retu	Profile(s) Duration(s) (mins) 60, rn Period(s) (years) Climate Change (%)	120, 180, 240, 360, 480, 600, 720,	Winter 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080 1, 30, 100 0, 0, 40					
US/MH PN Name	Event	Water Surcharged Flooded US/CL Level Depth Volume (m) (m) (m) (m³)	Pipe Flow / Overflow Maximum Flow Cap. (l/s) Vol (m³) (l/s	v				
S1.000 S1 120	minute 100 year Winter I+409	≥ 16.350 16.130    0.280   0.000	0.30 37.429 4.	3 SURCHARGED				
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Micro Drainage	Network 2016.1.1	1

## 100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

PN	US/MH Name			E	vent			US/CL (m)	Water Level (m)	Surcharged Depth (m)		Flow / Cap.	Overflow (1/s)		Pipe Flow (l/s)	Status
S1.001	S2	120	minute	100	year	Winter	I+40%	16.500	16.101	0.741	0.000	0.23		0.992	4.2	SURCHARGED
S1.002	s3	60	minute	100	year	Winter	I+40%	16.350	15.674	0.714	0.000	0.27		0.979	4.6	SURCHARGED
S2.000	S4	60	minute	100	year	Winter	I+40%	15.950	15.734	0.134	0.000	0.41		6.305	6.3	SURCHARGED
S3.000	S5	120	minute	100	year	Winter	I+40%	16.350	16.122	0.272	0.000	0.19		26.781	2.7	SURCHARGED
S3.001	S6	120	minute	100	year	Winter	I+40%	16.500	16.109	0.749	0.000	0.15		0.999	2.3	SURCHARGED
S3.002	s7	60	minute	100	year	Winter	I+40%	16.350	15.669	0.729	0.000	0.18		1.016	2.8	SURCHARGED
S4.000	S8	60	minute	100	year	Winter	I+40%	15.950	15.679	0.079	0.000	0.24		3.678	4.3	SURCHARGED
S1.003	S4	60	minute	100	year	Winter	I+40%	16.500	15.664	0.814	0.000	0.31		1.490	11.3	SURCHARGED
S1.004	S5	960	minute	100	year	Winter	I+40%	14.000	13.625	0.275	0.000	0.17		0.602	7.6	SURCHARGED
S5.000	S12	960	minute	100	year	Winter	I+40%	13.850	13.624	1.224	0.000	0.76		276.643	2.0	SURCHARGED
S1.005	S6	960	minute	100	year	Winter	I+40%	13.850	13.620	1.095	0.000	0.07		1.723	2.0	SURCHARGED
S1.006	S7	960	minute	100	year	Winter	I+40%	14.000	13.620	1.040	0.000	0.03		1.514	1.8	SURCHARGED





# Drainage - Flood Risk - Highways - Transport

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